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AN EVALUATION AND APPLICATION OF A DIGITAL
HYDROLOGIC SIMULATION MODEL TO AN IDAHO WATERSHED

A Thesis

Presented in Partial Fulfillment of the Requirement for the
DEGREE OF MASTER OF SCIENCE

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by

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July, 1973

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ABSTRACT

Watershed simulation models have many engineering applications in the areas of research and project planning and management. In this study the Kentucky Watershed Model, a Fortran version of the Stanford Watershed Model, was adapted for use in Idaho.

The model was applied and evaluated on the Palouse River near Potlatch, Idaho, a 317 sq.mi. watershed in northern Idaho. Daily flows were synthesized and plotted against recorded flows for the 1967-1968 and 1969-1970 water years. The synthesized annual water yield was found to be 7.34 and 13.59 inches respectively versus recorded values of 5.68 and 12.05 inches. A tendency to underestimate peaks early in the runoff season and to underestimate the spring recession was also observed. An adjustment to the valley precipitation estimate was made to account for orographic influences on the amount of precipitation received in the upper mountainous region of the watershed.

CHAPTER I
INTRODUCTION

DIGITAL SIMULATION CONCEPT IN WATERSHED HYDROLOGY

Hydrology, a branch of earth science, deals with the occurrence, movement and distribution of water either above, on or under the earth's surface.

The hydrologic regimes of streams and rivers provide the fundamental information used for the design, planning and operation of hydraulic engineering projects (Crawford and Linsley, 1966). Thus a thorough understanding of the hydrologic cycle and the water budget is a necessary condition for optimal utilization of the water resource on earth. In order to better perform this task, simulation techniques have been brought into this field recently utilizing the high-speed electronic digital or analog computer. Through the use of computers, an indirect investigation of the response and the behavior of the inter-relationships among the hydrologic components can be attained.

Dawdy (1969) stated, "One of the major aims of hydrology is to determine meaningful measures which describe a particular element of hydrology." These measures may be the response of floods, low flows, or parameters which describe the physical system. Simulation models are structured so as to contain within their parameters all the

information concerning these measures and responses. "A second major aim of hydrology is prediction." (Dawdy,1969). Examples are prediction of a flood from a snowpack or rain-storm and the prediction of response of an aquifer to certain withdrawals.

What is simulation? Simulation in general is a representation of reality. It is a technique by which complex systems can be analyzed with less difficulty and expense than would be required by manipulation of the prototype. In digital simulation in hydrology, the system is a collection of quantitative hydrologic concepts with mathematical representation in the form of a digital computer program. Such a system, or model, is usually designed to simulate streamflows over a preselected period of time. The input to the model is usually climatological, physical or geographical data for a specified watershed. If each of these concepts is well established and every physical component of the watershed is properly represented in the model, the entire model would be unique and all physical processes in the watershed could be accurately simulated (Crawford and Linsley, 1966).

STUDY OBJECTIVES

Crawford and Linsley of the Department of Civil Engineering, Stanford University have made a pioneering effort in modelling the hydrologic cycle through their development of the Stanford Watershed Model. It is the

purpose of this study to adapt the Kentucky version of the³
Stanford Watershed Model for use on the computer system
available at the University of Idaho, and to apply the
model to an Idaho watershed. It was in this context that
the study was initiated with these general objectives:

- (1) To study some basic concepts in watershed modelling.
- (2) To present a watershed model application in a document-
ary form that would allow later users to use the model
efficiently.

Some basic knowledge of hydrologic model building
and a brief review of those watershed models that already
exist was deemed necessary before proper, practical water-
shed simulation could be performed. Chapter II contains
this information along with a short description of the
Kentucky Watershed Model. Due primarily to limited storage
capacity of the IBM 360/40 computer at the University of
Idaho, changes and modifications of the computer program
were made. These are described in Chapter III. Chapter IV
contains a discussion of the simulation of a watershed in
Idaho, the selection of parameters and input data
justifications, and the presentation and discussion of the
results. Finally, conclusions and recommendations are
given in Chapter V.

CHAPTER II
LITERATURE REVIEW

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WATERSHED SIMULATION MODELS

The hydrologic cycle is fairly easy to describe in qualitative terms because the interactions between major components are well known. But the extension of this qualitative knowledge to obtain quantitative results is very difficult due to the fact that hydrologic processes are very complex, interrelated and strongly time dependent (Crawford and Linsley, 1966). The advent of the computer provided a valuable tool by which synthesized streamflow records can be obtained from a mathematical model with climatological data and physical characteristics of the study watershed as inputs. Watershed modelling consists of recognizing the various phases of the physical processes involved in the hydrologic cycle on a watershed and mathematically describing them as a continuous and dynamic system. Dawdy (1969) stated: "Quantitative estimates require modelling. The more closely the model approximates the system modeled, the more accurate is the prediction obtained by using the model." There is always a compromise between simplicity and accuracy of the model. The desirability of compromise is well documented in previous work and is based on minimizing both cost and effort. Model building is not a simple task. It may take several years to develop a model and thousands of man hours to use

(Dawdy, 1969). Such model building is both an art and a science. The science comes in the theoretical derivation and empirical verification of equations describing hydrologic phenomenon. The art comes in reviewing these available equations and supporting data, and estimating and adjusting certain parameters and calibrating the model in the manner which will give the best results (James, 1972).

The attempt to develop mathematical simulation models in hydrology is underlain by two basic assumptions which have been indicated by Dawdy (1969): "First is the belief that a properly designed and calibrated model will summarize the hydrology of any particular system, second is the belief that the model can be used for prediction either on a short term or a long term basis to extend the available data base." The following criteria or requirements are considered to be necessary in developing watershed models (Crawford and Linsley, 1966):

- (1) The model should include the complete hydrologic system.
- (2) It should be flexible enough to be easily applied to different watersheds with existing hydrologic data.
- (3) It should be sufficiently sensitive to reflect changes in output data when input parameters are modified.
- (4) The model should be physically relevant so that estimates of other useful data in addition

to streamflow can be obtained.

Crawford and Linsley made a pioneering effort to make watershed modelling practical for general use through their development of the Stanford Watershed Model at Stanford University beginning in 1959. They represented each process by an equation or series of equations containing parameters which vary in value for different watersheds and whose specific values are read in as input data. The model was structured in a general form which could be applied to all watersheds by using a set of parameter values which are found through trial and error by providing acceptable matching of simulated to recorded flows or measured moisture storage (James, 1972). The flexibility of the model allows the user to change or introduce equations freely to reflect new scientific information. The Stanford Watershed Model has been through four stages of development. Model I was developed in 1959, and considered only the elementary hydrologic concepts of a watershed. Model II was introduced in 1962 and included improvements and revisions that were incorporated into Model I. Model III was released in 1964 followed by Model IV in 1966. Model IV differs from model III in that the input data have been simplified, adjustments have been made in some moisture routing equations, and runoff has been combined from sub-watersheds into a common hydrograph (Ligon and others, 1969).

Ever since the appearance of the Stanford Watershed Model, others have adapted this model to their own research or application needs. Many have modified the program and translated the language for use in their local computer facilities. Others have attempted to increase program capabilities or extend the printed output for additional information. For the past few years, published reports have shown that these sorts of efforts have been made at Kentucky University (James, 1970); Clemson University, South Carolina (Ligon and others, 1969); Virginia Polytechnic Institute and State University, Virginia (Shanholtz and others, 1971; Shanholtz and Lillard, 1971); Soil Conservation Service, Portland, Oregon (Rallison, n.d.); and at Ohio State University, Ohio (Ricca, 1972). Other than the above Stanford-type watershed models, there are many similar models which have subsequently been developed both in government agencies and in universities, which have made notable contributions to watershed hydrology. Among these are: TVA Continuous Daily-streamflow Model (TVA, 1972); Indiana Watershed Runoff Estimation Model (Lee and Delleur, 1972); and USDAHL-70 Model (Holtan and Lopez, 1971).

In addition to digital simulation, electronic analog computers also have been employed for modelling particular problems for which they are most appropriate. In 1960, the Hydraulic Laboratory of the University of California built an analog model for the purpose of routing

floods in a particular river system (Riley and Chadwick, 1967). Research in electronic analog models of hydrologic systems began at Utah State University in 1963 and such a device was subsequently designed and built in 1964. An analog computer program has been developed for simulating flood conditions on the Kitakami River of Japan in 1965 (Riley and Chadwick, 1967). The electronic analog computer has several important advantages in simulating the hydrologic phenomena as indicated by Riley and Chadwick (1967):

- (1) It behaves electronically in a manner analogous with the problem solved. If problem size doubled, the amount of analog equipment required also doubled but the time, for solving the problem remains the same.
- (2) Many processes occur in nature are time-dependent and are differential in form. Analog computers are able to integrate problem variables continuously instead of using numerical approximation.
- (3) Because of the capability for continuous output feedback during problem solving, program optimization can be undertaken on the analog computer during the computation process.

Although the analog computer has the aforementioned advantages in simulation of hydrologic phenomena, digital

simulation is still the most widely used method due to the wider availability and large storage capacity of the digital computer.

THE KENTUCKY WATERSHED MODEL

One of the major difficulties of using the Stanford Watershed Model is the programming language. The original program was written in the SUBALGOL language (Stanford University modification of the Burroughs Corporation ALGOL language) used by the Stanford Computer Center. Douglas L. James of the University of Kentucky has translated and modified the model into FORTRAN IV language. The differences which exist between the Stanford Model and the Kentucky Model are the addition of input data simplifications, the use of a revised procedure for reading storage gage rainfalls, and the addition of a section for printout of daily soil moisture (Ligon and others, 1969).

The model upon which this study was based is the latest version (dated June 6, 1970) of the Kentucky Watershed Model where minor reprogramming has been done to increase computational efficiency, to introduce some new

options, and to revise output format. This Kentucky Watershed Model is composed of one master program (MAIN) and seven subroutine programs. The MAIN controls operations as directed by coded control options, performs the moisture accounting process to synthesize flows, calls subroutines and handles program output. The input data required for a computer run may be divided into the following six groups:

- (1) Data used to title the watershed, to identify the computer run, to specify the desired program options and to request specific output. Fourteen values of these control options which select the program features the user wishes to use are listed in TABLE 2-1.
- (2) Time-area histogram data.
- (3) Data to describe climatological events during the water year.
- (4) Data to initialize watershed moisture storage starting October 1 of the first water year being synthesized.
- (5) Values for watershed parameters either measured or estimated by the user.
- (6) Daily recorded streamflow data for the purpose of correlating the recorded and synthesized flows.

TABLE 2-1 Definition of the optional control code used
in the Kentucky Watershed Model

CONOPT	Code	Definition
1	1	program prints out 15-minute storm details.
	0	program does not print out these values.
2	1	hourly rainfall is to be divided equally into 15-minute periods.
	0	hourly rainfall is not to be divided equally into 15-minute periods.
3	1	program reads in average daily evaporation during 10-day periods.
	2	program reads in average annual lake evaporation and the average annual number of recorded rainy days.
	0	program reads in 365 or 366 daily pan evaporation totals and monthly pan evaporation coefficient values.
4	1	program prints out daily flow error table at end of year.
	0	program neither calculates nor prints out these values.
5	1	program prints out 20 top hourly rainfall and runoff values during the year.
	0	program does not print these values.
6	1	program prints daily values of soil moisture storage.
	0	program does not print these values.
7	1	program reads in additional snow data.
	0	program treats all precipitation as rainfall.
8	1	program accepts input from more than one recording rain gage.
	0	program accepts only one recording gage.

TABLE 2-1 (continued)

CONOPT	Code	Definition
9	1	program reads in 365 or 366 daily recorded streamflows.
	0	program does not read in these values.
10	1	program will read new watershed parameters.
	0	program will not read these data.
11	1	program reads in daily values of diverted flow in cfs.
	0	program does not read in these values.
12	1	program routes streamflow on an hourly basis.
	0	program routes streamflow on 15-minute basis.
13	1	the length of time-area-histogram is to be varied with flow velocity.
	0	the length is not to be varied with flow velocity.
14	1	program prints daily recorded streamflows.
	0	program does not print these records.

Subroutine READ is employed to read numerical input data from punched data cards. READ is specially developed for free input data format with explanatory messages and is written in computer machine language for the IBM 360/65.

Subroutine DAYOUT prints a table of daily values given the magnitude of each desired value, the day of the year of the last day of each month, and the number of days in the year. It converts values arranged by calendar-year

day into the water-year month order printout.

Subroutine EVPDAY uses regional data to distribute a total annual evaporation over the days of the year. According to the type of data the user has available, he can choose from among three approaches to read the necessary information as specified by control option 3.

Subroutine PREPRD divides precipitation among the 15-minute periods using the average distribution approach.

Subroutine RTVARY is used for varying stream routing time according the streamflow magnitude.

Subroutine SNOWMELT is used for the calculation of runoff and evaporation from snow when snowfall is a significant part of the precipitation of an area.

A watershed can be visualized as an open physical system with precipitation as input and streamflow as output (FIGURE 2-1). The logic concept of the computer program is based on a moisture balance within the watershed boundary, where all precipitation falling on the watershed is accounted for until it evaporates or flows out of the watershed.

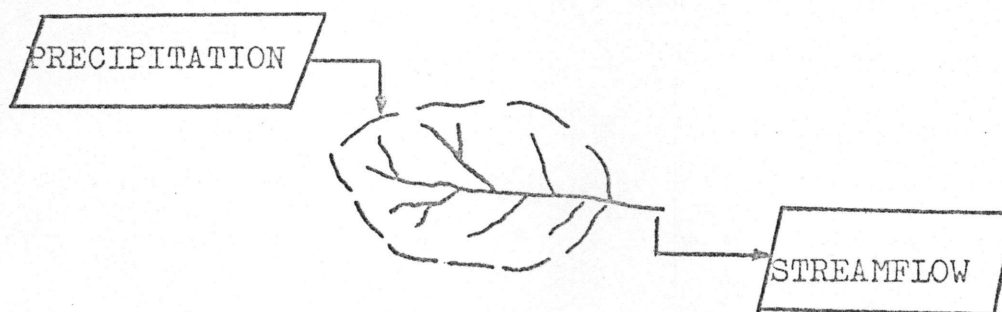


FIGURE 2-1 Watershed as an open physical system

FIGURE 2-2 is a schematic diagram of the operation of the hydrologic cycle in the Stanford Watershed Model (Crawford and Linsley, 1966). Each box represents a hydrologic component or a classification of moisture storage. The arrows represent processes whereby moisture moves from one type of storage to another (James, 1972). Precipitation and potential evapotranspiration are the major data inputs. Additional data are needed if snowfall is included in the model. Precipitation is first subjected to interception, then stored in the snowpack and in three soil moisture storages - upper zone storage, lower zone storage and groundwater storage. Precipitation falling on impervious areas contributes directly to the channel inflow. The upper zone and lower zone storage control the overland flow, interflow, infiltration and percolation to the ground water storage. Evaporation and transpiration may occur from all of these storages and remove water from the watershed. The moisture accounting period is 15-minutes. The total channel inflow from impervious areas, overland flow, interflow and groundwater flow is then routed to the watershed outlet by the time-area routing method and the result is simulated streamflow.

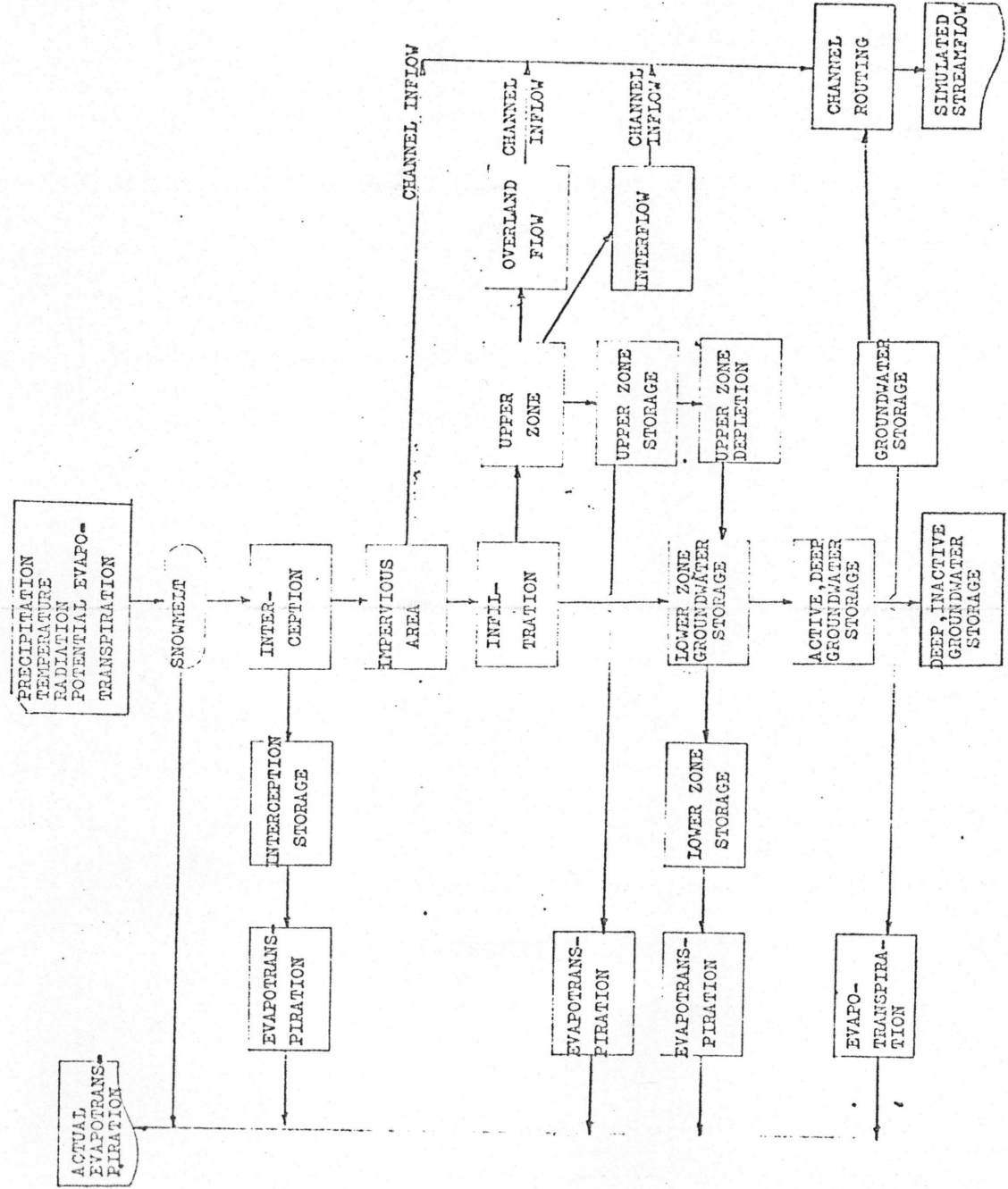


FIGURE 2-2 Schematic diagram of the operation of Stanford Watershed Model

CHAPTER III

CHANGES INCORPORATED INTO THE KENTUCKY WATERSHED MODEL

The model employed in this study was the Kentucky version of the Stanford Watershed Model (or Kentucky Watershed Model). This particular model was used simply because the program deck is readily available and the model itself is considered general enough to be applied to watersheds in the western states. In order to operate this model on the IBM 360/40 computer currently available at the University of Idaho, some changes and modifications of the program were made. The primary effect of the modifications was reduction in the storage requirement and the execution time. During experimental runs, minor improvements which appeared to be beneficial were also incorporated into the program. These are described in the following paragraphs. The program presently (as of June, 1973) in operation consists of one MAIN program and five subroutines. The changes that have been made are summarized below:

SUBROUTINE READ

Subroutine READ in the original program was written in machine language for IBM 360/65. This subroutine is now replaced by conventional FORTRAN IV read statements. Consequently, revision of the associated input data format was required. This change introduced more difficulty in data

preparation and also added more computer run time. Special care should be exercised in arranging the input data. Data cards must be arranged in a sequence that can be read in according to the particular control option used within the program.

SUBROUTINE EVPDAY

To reduce the storage requirement, subroutine EVPDAY was removed from the program. As a consequence, the use of "2" in control option 3 was eliminated. This means that the program must read in daily evaporation data either as averages over ten-day periods or as 365 or 366 daily pan evaporation items with monthly pan evaporation coefficient values.

PROGRAM TERMINATION

Program termination statements were revised to give additional control. The original program terminated upon reaching the END-OF-FILE card and in turn printed out error messages. To eliminate error messages new statements were inserted to cause exit when end of record was read.

At the beginning of the program, the number of years of recorded data to be input is read in by the following statements.

C READ IN NUMBER OF YEARS OF RECORDED DATA REQUIRED

READ(5,2050) NOYR

```
2050  FORMAT(I2)
```

At the end of the program, a counter is set up and is checked to direct the program whether to go back to start a new year or to terminate the program:

```
NOYR=NOYR-1  
IF(NOYR.EQ.0) GO TO 117
```

With this added capacity, any number of years records can be simulated.

ADDITIONAL CONTROL OPTION TABLE PRINTOUT

For the convenience of correlating the program printout with the options specified, the following statements were added to print out the control option table:

```
WRITE(6,998)  
998  FORMAT('1',15X,'CONTROL OPTION CODE TABLE')  
DO 99 J=1,14  
99  WRITE(6,999) CONOPT(J),J  
999  FORMAT(/50X,'* ',I2,' * OPTION ',I2,' *')
```

This printed table permits the user to easily correlate the program output with that particular set of control options

used without going back to the data deck. The meaning of each code can be found in Chapter II Table 2-1. A sample printout is presented below:

CONTROL OPTION CODE TABLE

*	1	*	OPTION	1	*
*	0	*	OPTION	2	*
*	1	*	OPTION	3	*
*	1	*	OPTION	4	*
*	0	*	OPTION	5	*
*	0	*	OPTION	6	*
*	0	*	OPTION	7	*
*	0	*	OPTION	8	*
*	1	*	OPTION	9	*
*	0	*	OPTION	10	*
*	1	*	OPTION	11	*
*	1	*	OPTION	12	*
*	0	*	OPTION	13	*
*	1	*	OPTION	14	*

CHAPTER IV
APPLICATION TO AN IDAHO WATERSHED

One of the objectives of this study was to evaluate the effectiveness of the Kentucky Watershed Model in predicting the streamflow from a watershed in Idaho. The Palouse River near Potlatch was selected for this application.

GENERAL DESCRIPTION OF THE STUDY WATERSHED

The Palouse River watershed near Potlatch (FIGURE 4-1) is located in Latah and Benewah Counties in northern Idaho. It is situated approximately 18 miles north of Moscow, Idaho in the St. Joe National Forest. The mountains are spurs and bordering ridges of the Coeur d' Alene Mountain division of the northern Rocky Mountains.

Bedrock strata in the basin are of the Precambrian Belt Supergroup; these are principally older rocks consisting of argillites, silty argillites, and some quartzites. This type of bedrock prevails downstream through the Laird Park area on the main stem. Boulders, cobbles, gravels and substrate in the main river and its tributaries are of this nature. Similar loose rock underlying the broad flood plain continue to a point just east of Princeton. At this point lava flows of the Columbia River Group, form a basaltic bedrock stream floor at places with gravel and silty

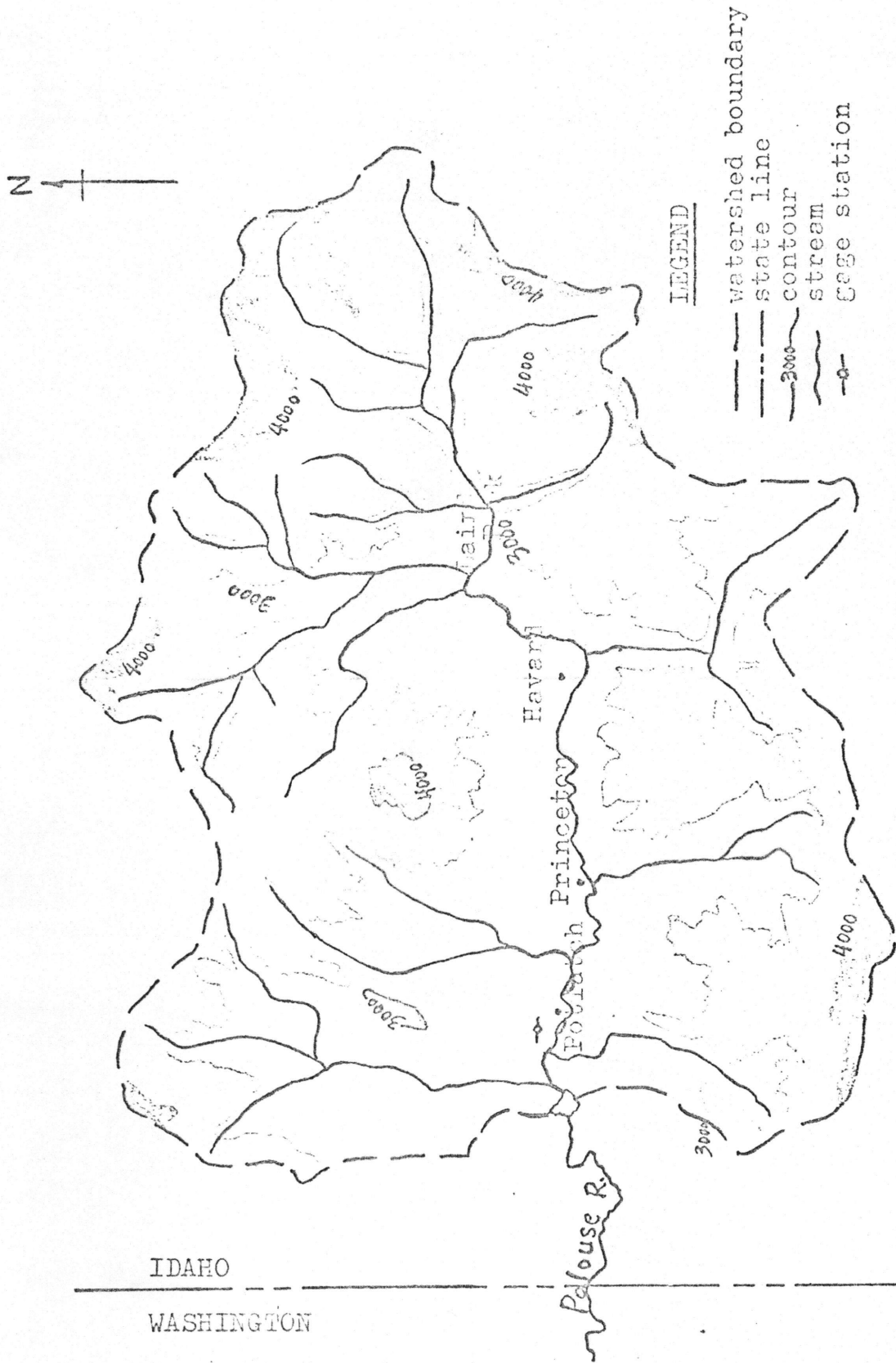


FIGURE 4-1 The Palouse River near Potlatch watershed

sand substrate other places to Potlatch. Loess covers the area from Laird Park downward with increasing thickness toward the lower end. This material contributes considerable silt in the streams at some times of the year. The watershed eventually drains into the Snake River, and subsequently into the Columbia River.

Land slopes of the watershed are moderate to steep with an elevation range of 2480 ft to 5060 ft above sea level. The climate is temperate with average annual temperature of 45°F. The average annual precipitation is 25 inches mostly in fall, winter and spring month. Snowfall is the major form of precipitation during the winter months. The principal source of moisture is the Pacific Ocean and weather patterns move generally from west to east. The higher elevations are forest covered while cropland with interspersed timber is the major land use in lower elevations. Detailed soil survey have been made by the Soil Conservation Service and by Clark, Coleman and Rupeiks Inc. Seattle, Washington. The general soil characteristics of the area are summarized in TABLE 4-1. Some of the physiographic characteristics of the watershed are summarized below:

Drainage area: 317 sq.mi.

Elongation ratio: 0.576

Total watershed relief: 2580 ft.

Drainage density: 1.65 mi./sq.mi.

TABLE 4-1 Summary of general soil characteristics of Palouse River watershed

Soil Type	Watershed Area (%)	Depth (inches)	Available Water Capacity (inches)	Natural Drainage
Helmer Silt Loam	2	60	8-11	Somewhat poor
Huckleberry Stony Silt Loam	37	20-40	5-8	Good
Minaloose Gravelly Loam	29	20-40	4-7	Good
Santa Silt Loam	10	60	6-9	Moderately good
Stanford Silt Loam	4	60	5-8	Somewhat poor
Taney Silt Loam	4	60	6-9	Moderately good
Uvi Silt Loam	3	20-40	5-8	Good
Vassar Silt Loam	11	40-60	6-9	Good

Average mean channel slope: 0.5%

Total stream length: 510 miles

The streamflow was simulated at the point where the stream gage is located at latitude of $45^{\circ}54'55''$ North, longitude $116^{\circ}57'00''$ East in Latah County, on the left bank 20 feet down stream from a bridge on U.S. Highway 95, 1.0 mile downstream from Deep Creek, 2.0 miles west of Potlatch. The average annual discharge for eight years of record is 265 cfs (or 11.35 inches of runoff) with a maximum discharge of 51,910 cfs and a minimum of 1.2 cfs. Non-recording temperature and precipitation gages are located 3 miles NNE of Potlatch, at latitude $46^{\circ}58'$ North and longitude $116^{\circ}53'$ East.

PREPARATION OF INPUT DATA

One of the major problems in the application of a watershed model is the collection of the required input data and the determination of parameter values. Suitable determination of watershed parameter values is the key to the successful application of a watershed model. When a user applies the model to a watershed, he must collect the necessary meteorological data from historical records, measure the required soil and physiographic watershed characteristics, estimate proper values for certain parameters, and then adjust these parameter values by trial-and-error methods until a certain degree of accuracy is

attained. These adjustments and calibrations are the art of modelling. It requires familiarity with the model employed and some understanding of the sensitivity of the parameters under study. In using the Kentucky Watershed Model, this process is greatly aided by studying recently published reports written by James (1970), Ross (1970) and Liou (1970). However, the decision of selecting a final set of parameter values is essentially subjective. Ross (1970) presented the set of parameters used in the Kentucky Watershed Model in a schematic diagram shown in FIGURE 4-2. The underlined parameters are those which were not measurable. The following table gives the range of values for each parameter used in the Kentucky Watershed Model.

<u>Parameter name</u>	<u>Range of value</u> *	<u>Reference or source</u>
FIMP	0-1	Ross (1970) p.40
VINTMR	0.01-0.20	Ross (1970) p.40
GWETF	usually 0	Ross (1970) p.40
SUBWF	usually 0	Ross (1970) p.41
OFMN	0.009-0.200	V.T.Chou (1959) Open Channel Hydraulics p.110-113
OFMNIS	0.013-0.100	Ross (1970) p.44
IFRC	0.100-0.620	Ross (1970) p.87; James (1970) p.48
BFRC	0.722-0.9967	Ross (1970) p.87; James (1970) p.48
BFNLR	0.9-1.0	Ross (1970) p.47
ETLF	0.20-0.30	Ross (1970) p.53
SIAC	0.15-0.70	Ross (1970) p.115
BMIR	1.12-21.85	Ross (1970) p.130,131; James (1970) p.46

<u>Parameter name</u>	<u>Range of value</u>	<u>Reference or source</u>
BIVF	0.0-3.91	Ross (1970) p.87
CSRX	0.887-0.962	Ross (1970) p.87
FSRX	0.900-0.990	Ross (1970) p.87; James (1970) p.48
EXQPV	0.1-0.25	Ross (1970) p.24
BUZC	0.43-7.42	Ross (1970) p.87
SUZC	0.35-2.04	Ross (1970) p.87
LZC	2.03-28.05	Ross (1970) p.87

* Values taken mainly from Kentucky state.

Without doubt, prior knowledge of the expected direction and magnitude of responses to selected changes in input data, is helpful in minimizing the number of trials required to obtain an optimal set of input values. This was accomplished in this study by numerous simulation runs using Elkhorn Creek data from Kentucky. Such parameters as ETLF, LZC, SIAC, VINTMR, BIVF, BMIR were given particular attention since they are more sensitive than others as indicated by Ross (1970). Each parameter was changed, either alone or with several others, and the effect of this change on the simulated streamflow was noted. When it was felt that sufficient experience had been gained in operating the model, the model was applied to the Palouse River near Potlatch.

The application to the Palouse River logically began with the collection of data. This data collection

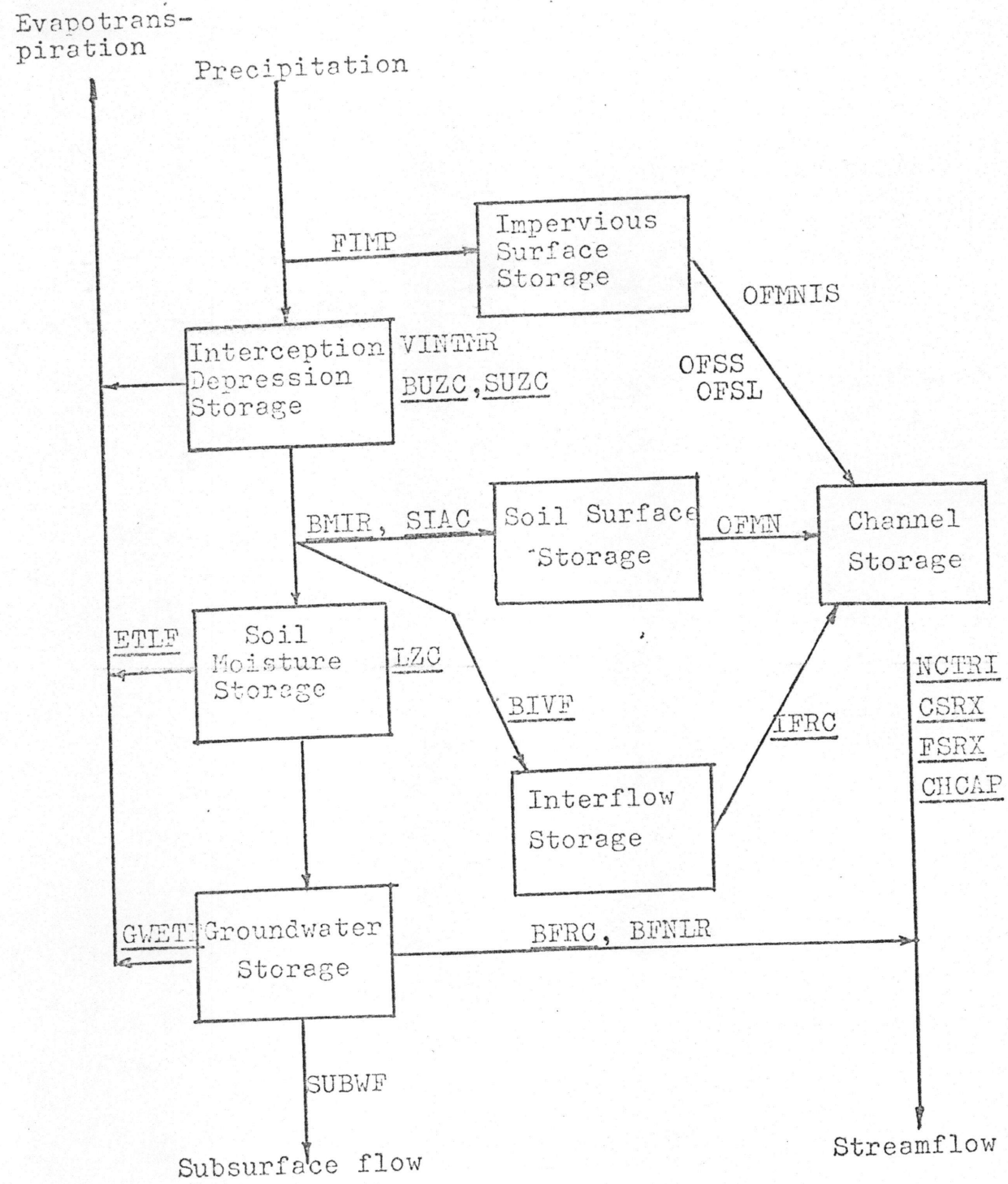


FIGURE 4-2 Schematic diagram of the parameters used in the Kentucky Watershed Model

was divided into three groups:

Group I Recorded climatological data- such as precipitation, evaporation, temperature, radiation, etc. can be obtained from the monthly publication of U.S. Department of Commerce, National Oceanic and Atmospheric Administration, Environmental Data Service. Daily streamflow data can be obtained from the Surface Water Records published by United States Department of the Interior, Geological Survey.

Group II Measurable or assignable parameter data- such as AREA, RMPF, FIMP, FWTR, OFSS, OFSL, OFMN, EPCM, CTRI, NCTRI, CHCAP, etc. are obtainable from a topographic map or from a knowledge of the watershed.

Group III Estimated data- such as IFRC, BUZC, SUZC, LZC, ETLF, SIAC, BMIR, CSRX, FSRX, etc. These parameters can be estimated initially from whatever physical and hydrologic data are available or with reference to other similar watersheds. Further adjustments are required based on the feedback from trial simulations.

Difficulty was encountered in finding hourly precipitation data. The Potlatch rain gage is of the non-

recording type read once per day. However, a gage at Plummer, 30 miles north of Potlatch, did have hourly data. Therefore, the precipitation at Potlatch was distributed throughout each precipitation period in the same ratio as the precipitation at Plummer. After the input data were collected, a few initial trial runs were conducted to examine the effects of parameter variations. Most attention was given to the evapotranspiration loss factor, the soil moisture storage index, the base flow recession constant, the interflow volume factor and the seasonal infiltration adjustment constant. Attempts were made to manipulate these parameters in order to obtain a better match between synthesized and recorded streamflows. Computerized optimization techniques have been devised to substitute for the manual approach used in this work. Owing to the limitation of the available computer facilities, it was not possible to use such techniques in this study. For the first trial run, the synthesized annual runoff was 6.64 inches which was very low compared to the recorded annual runoff of 12.05 inches. Since increasing the interflow volume and decreasing the infiltration rate will increase the total runoff, the value of BIVF was changed from 3.5 to 5.0 and BMIR was changed from 6.0 to 4.0 in the second trial run. This increased the synthesized annual runoff to 6.84 inches with the correlation coefficient (r) equal to 0.8323 as

opposed to an r value of 0.8416 for the first trial. In the third trial run, the value of LZS was increased from the initial estimated value of 2.0 to 5.0. Increasing the LZS value increases the soil moisture ratio, LZS/LZC, which in turn will increase the interflow volume and the total annual runoff. After this trial run, the synthesized annual runoff was increased to 8.94 inches. However, the r value was decreased to 0.8071. The changes involved in the fourth trial run were to decrease the seasonal infiltration adjustment constant, SIAC, which should increase runoff in summer; to increase the base flow recession constant, BERC, which should reduce the peak recession rate; to decrease the evapotranspiration rate, ETLF, which should increase the total runoff. The synthesized total annual runoff obtained from this trial run was 8.69 inches and the correlation coefficient between synthesized and recorded streamflows was 0.8214. The results and the set of parameter values chosen for this particular run will be presented later in this chapter.

FURTHER ADJUSTMENT OF PRECIPITATION

In comparing the outflow hydrograph obtained from the fourth run, it was observed that the simulated annual streamflow (8.69 inches of runoff) was lower than that of the recorded (12.05 inches). The simulated monthly flows were also low in general but especially in summer months. The timing of the peaks seemed to match fairly well, but the recession rate was too high. Since the only source of moisture is precipitation, attention was then drawn to the justification of the input precipitation. The precipitation records used in the model input were from a single rain gage located at the watershed outlet, the lowest elevation in the drainage. For more accurate representation of the precipitation amount over the entire watershed, it was decided that consideration should be given to the variations of precipitation distribution at different elevations in the basin. Rationale for this precipitation adjustment was supplied by Bloomsburg (1958). This study develops an elevation-precipitation relationship from isohyetal and contour maps for Crumerine and Gnat Creek watersheds near Moscow. These watersheds are approximately 12 miles from the study watershed and although smaller, have about the same relief and aspect. Taking the base point as having 100% precipitation, Bloomsburg used the following precipitation-elevation correction:

which increased the synthesized annual total runoff to 13.59 inches. At this stage, efforts were then concentrated in adjusting such parameters as SIAC, BIVF, BMIR and LZS to increase runoff in summer and to reduce peak recessions for better agreement between simulated and recorded flows. An additional verifying run was conducted for the 1967-1968 water year.

PRESENTATION OF RESULTS AND DISCUSSION

In this section, the simulation results of the application of the model to the Palouse River near Potlatch watershed are presented. As has been mentioned earlier several trials were required before a visually acceptable fit of the simulated and recorded hydrographs was obtained. This is admittedly a subjective procedure but it is widely used in hydrology. It also allows the hydrologist to concentrate on those parts of the annual hydrograph which are of interest to him. Undoubtedly a finer fit could be made if given sufficient time and efforts. TABLE 4-2 gives the parameter values selected for water year 1969-1970 before and after the adjustment of precipitation. Definitions of the parameters are given in Appendix A, Dictionary of Program Variables. TABLE 4-3 and FIGURE 4-3 show the comparison of the monthly synthesized streamflows with recorded streamflows and the daily streamflow hydrograph respectively for 1969-1970 before the precipitation adjust-

TABLE 4-2 Summary of parameter values for Palouse River near Potlatch watershed before and after the adjustment of precipitation

Parameters	Values prior to precipitation adjustment	Values after precipitation adjustment
<u>Snowmelt</u>		
BDDFSM	0.002	0.002
SPBFLW	0.05	0.05
SPTWCC	2.5	2.5
SPM	1.2	1.2
ELDIF	0.5	0.5
XDNFS	0.05	0.05
FFOR	0.65	0.65
FFSI	0.03	0.03
MRNSM	0.0126	0.0126
DSMCH	0.02	0.02
PXCSA	0.2	0.2
<u>Watershed</u>		
RGPMB	1.0	1.0
AREA	317.0	317.0
FIMP	0.0	0.0

Parameters	Values prior to precipitation adjustment	Values after precipitation adjustment
FWTR	0.0	0.0
<u>Overland flow</u>		
OFSS	0.29	0.29
OFSL	1500.0	1500.0
OFVN	0.050	0.050
OFVNIS	0.015	0.015
IFRC	0.40	0.40
<u>Initial moisture storage</u>		
GWS	0.02	0.02
UZS	0.0	0.0
LZS	4.0	4.0
BFNX	0.02	0.02
IFS	0.0	0.0
<u>Soil moisture</u>		
VINTMR	0.15	0.15
BUZC	1.0	1.0
SUZC	0.60	0.60

TABLE 4-2 (continued)

Parameters	Values prior to precipitation adjustment	Values after precipitation adjustment
LZC	6.5	7.4
ETLF	0.27	0.27
SUBWF	0.0	0.0
SIAC	0.50	0.30
BMIR	4.0	6.0
BIVF	5.0	5.5
<u>Channel routing and groundwater</u>		
CSRX	0.95	0.95
FSRX	0.97	0.97
CHCAP	2000.0	2000.0
EXQPV	0.25	0.25
BFNLR	1.0	1.0
BFRC	0.85	0.85

TABLE 4-3 Monthly synthesized and recorded streamflows
for water year 1969-1970 before precipitation
adjustment

Month	Synthesized (cfs-days)	Recorded (cfs-days)	Difference (%)
Oct.	291.1	387.3	+24.8
Nov.	154.8	418.9	+63.1
Dec.	2689.6	1335.8	-101.4
Jan.	25454.5	21994.0	-15.7
Feb.	19619.5	25376.0	+22.7
Mar.	15817.1	21334.0	+25.9
Apr.	7489.0	15658.0	+52.2
May	1570.0	12154.0	+87.1
Jun.	669.7	2517.0	+73.4
Jul.	224.0	810.0	+72.4
Aug.	79.7	309.8	+74.3
Sep.	5.8	388.1	+98.5
TOTAL	74064.8	102682.8	+27.8

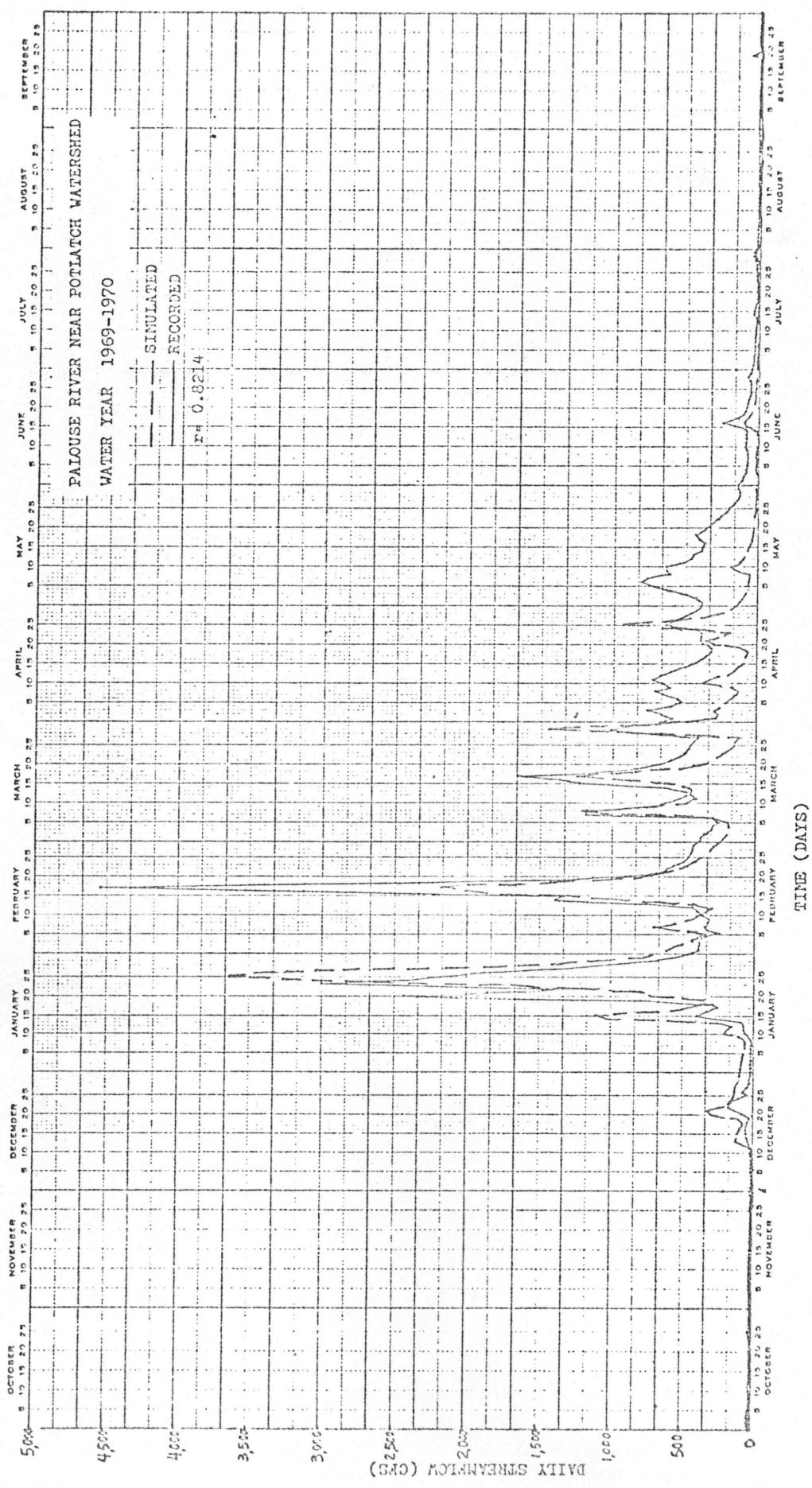


FIGURE 4-3 Daily streamflow hydrograph for water year 1969-1970 before precipitation adjustment

ment was made. TABLE 4-4 and TABLE 4-5 show the monthly synthesized and recorded streamflows for water year 1969-1970 and water year 1967-1968 respectively. The daily streamflow hydrographs for water year 1969-1970 and 1967-1968 are also presented in FIGURE 4-4 and FIGURE 4-5 respectively.

In evaluating the accuracy of the model output, a visual examination of plotted hydrographs is a reliable method. But it is somewhat subjective in most instances. The use of the linear correlation coefficient between synthesized and recorded flows, for example, gives an objective indication of the response of one value relative to another. The error table from the computer printout summarized the events occurring at preselected flow intervals over the period of analysis, and the standard errors were also calculated for each respective interval.

It was observed that the precipitation adjustment was necessary in order to better represent the average precipitation over the entire watershed. The results shown did indicate that this adjustment was appropriate. Other than precipitation, a few parameters also control the synthesized monthly and annual yields. These are the parameters related to the infiltration and soil moisture storage factors, such as LZC (lower zone capacity), LZS (lower zone storage), and BMIR (basic maximum infiltration rate) were found particularly sensitive to surface runoff.

TABLE 4-4 Monthly synthesized and recorded streamflows for water year 1969-1970 after precipitation adjustment

Month	Synthesized (cfs-days)	Recorded (cfs-days)	Difference (%)
Oct.	310.6	387.3	+19.8
Nov.	261.1	418.9	+37.7
Dec.	3240.0	1335.8	-142.6
Jan.	27756.6	21994.0	-26.2
Feb.	28659.0	25376.0	-12.9
Mar.	22946.3	21334.0	-7.6
Apr.	10372.5	15658.0	+33.8
May	3208.4	12154.0	+73.6
Jun.	2090.8	2517.0	+16.9
Jul.	1149.2	810.0	-41.9
Aug.	455.8	309.8	-47.1
Sep.	23.9	388.1	+93.8
TOTAL	100473.9	102682.8	+2.2

TABLE 4-5 Monthly synthesized and recorded streamflows
for water year 1967-1968

Month	Synthesized (cfs-days)	Recorded (cfs-days)	Difference (%)
Oct.	455.0	418.0	-8.8
Nov.	898.0	513.3	-75.0
Dec.	8850.9	2409.0	-267.4
Jan.	6672.5	2332.0	-186.1
Feb.	31261.3	27798.0	-12.5
Mar.	10176.6	6843.0	-48.7
Apr.	2487.6	4659.0	+46.6
May	596.8	1662.0	+64.1
Jun.	283.0	784.0	+63.9
Jul.	48.9	222.1	+78.0
Aug.	3.9	161.5	+97.6
Sep.	822.0	614.3	-33.8
TOTAL	62556.6	48417.1	-29.2

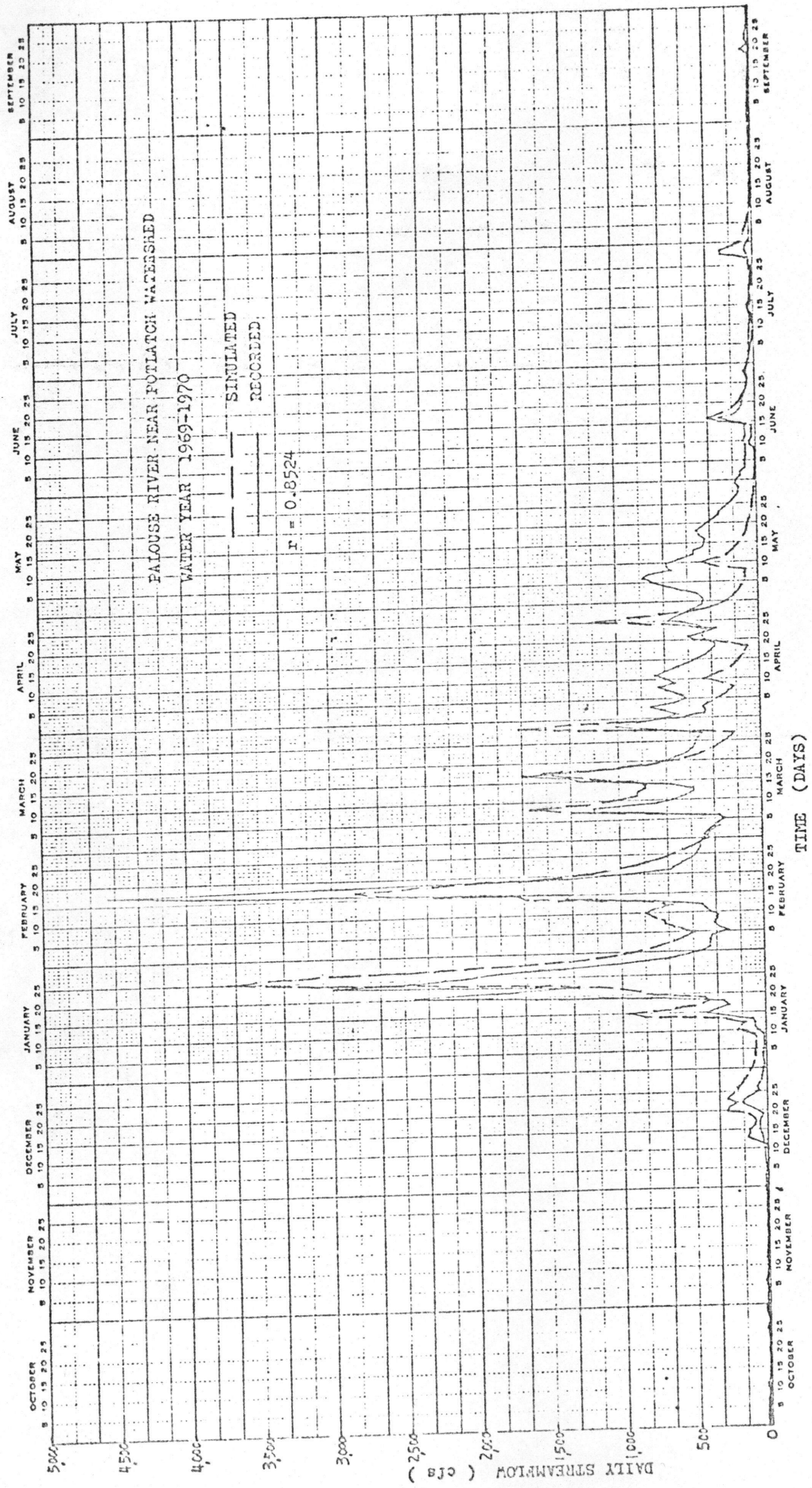


FIGURE 4-4 Daily streamflow hydrograph for water year 1969-1970 after precipitation adjustment

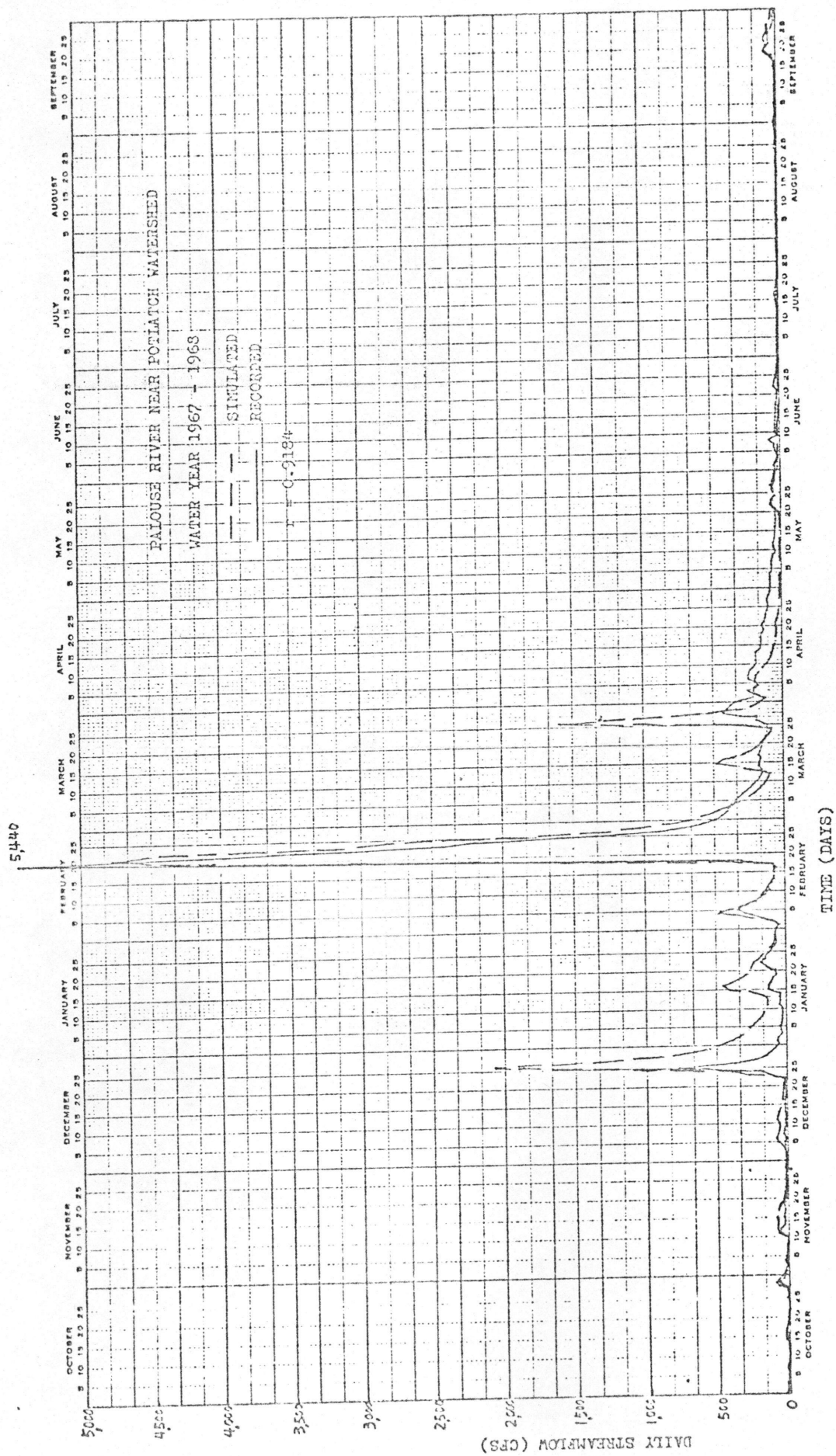


FIGURE 4-5 Daily streamflow hydrograph for water year 1967-1968

If LZC is decreased and LZS is increased, the annual water yield will also increase while an increase in MBIR will reduce runoff during storm periods. CSRX (channel storage routing index), FSRX (flood plain storage routing index), BIVF (basic interflow volume factor) were found more responsible for flood peaks. An increase in CSRX will result in a decrease in small flood peaks while an increase in FSRX will result in a decrease in large flood peaks. If it is desired to both reduce storm peaks in general and also extend the recession limb, then BIVF should be increased. The correlation coefficient, r , is 0.8524 for water year 1969-1970 and 0.9184 for water year 1967-1968. The agreement is considered acceptable for most months, although there were a few discrepancies in some months and peak discharges. In particular, the synthesized runoff in the early portion of winter is overestimated while the spring runoff is underestimated. There are exceptions to this in some spring peaks which are overestimated while their recessions are greatly underestimated. Additional manipulation of some parameters could lead to some improvement in matching the flood peaks. An explanation of these discrepancies could be due to large spatial and temporal variation of some storms over the watershed. The lack of accuracy of the potential evapotranspiration data and the snowmelt routine might explain the low simulated monthly volumes in spring and summer. The model accuracy also could be

affected by the assumption that watershed characteristics are evenly distributed throughout each time-area element. Any exception to this assumption could cause the departures between synthesized and recorded streamflows. Heterogeneous watersheds with different climatological and physiographic characteristics could be handled by subdividing the watershed into subdrainages or subwatersheds, and combining the results for each subwatershed to obtain the final hydrograph.

In conducting the analysis of the accuracy of the model output, two factors should be remembered. "First, the adequacy of the rainfall network to correctly represent the rainfall on the watershed, and second, the accuracy of the stream gage recording watershed response." (Crawford and Linsley, 1966). In most cases, the precipitation pattern is the major cause of departure of synthesized from recorded flows. There is no point in attempting to improve the accuracy of simulation beyond the accuracy of the input rainfall data.

CHAPTER V

CONCLUSIONS AND RECOMMENDATIONS

CONCLUSIONS

The model application and evaluation were made on the Palouse River near Potlatch in Idaho. During the application, difficulty was encountered in collecting the hourly precipitation data for the watershed, and in obtaining a set of values for the model parameters that would give the best fit of the outflow hydrograph. Considerable understanding of the model is necessary before a proper, practical application can be made to a watershed. Simulation techniques permit investigation of the effect of specific changes within the system being synthesized. Some conclusions are summarized as the result of this study:

1. The Kentucky Watershed Model can be adapted to operate on the IBM 360/40 digital computer at the University of Idaho.
2. The results of application of the model to an Idaho watershed are documented and presented. The model appears to reproduce the daily hydrograph within the accuracy of basic input data.
3. The application of the model to Idaho conditions seems feasible.
4. More study is necessary on the effect of precipitation variation over the basin on the simulated hydrograph.

In mountainous terrain, it may be necessary to divide the watershed into subwatersheds in order to account for this variation.

RECOMMENDATIONS

With the present level of understanding and the experience gained through the use of the Kentucky Watershed Model, the following recommendations are given:

1. A further break down of the main program into several subroutines seems necessary in order to provide an easier investigation of each hydrologic component.
2. The means of input data could be greatly simplified by using the free format input routine available at the Idaho Computer Center.
3. For a watershed with a single rain gage, the effect of errors in the measurement of watershed average rainfall should be given further investigation.
4. Calibration of the model should be extended to more watersheds with different physiographic and meteorological conditions where data are available. Watersheds selected from southern Idaho should be included in this analysis.
5. Attention should be given to selecting the proper watershed parameters for each watershed under study.
6. The model needs to be modified to include the effect of urban development within the watershed.

7. Further research could be done in developing better relationships between model parameter values and the physical watershed characteristics for easier usage of the model.

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<u>ELEVATION (FT)</u>	<u>PRECIPITATION (%)</u>
4000	200
3500	170
3000	140
2800	120
2700	110
2600 less	100

Adapting these data to the Palouse River watershed, the approximate average percentage of the precipitation over the entire watershed with respect to the base point was calculated as below:

<u>ELEVATION (FT)</u>	<u>AREA (%)</u>	<u>PRECIPITATION (%)</u>	<u>WEIGHTED PRECIP. (%)</u>
4000 up	8	200	16
3000-4000	45	170	76
2600-3000	41	120	49
2600 less	6	100	6

TOTAL: 147

Adjustment was then made to increase the input hourly precipitation data by the amount of 147%. However, results showed that this amount of precipitation was giving too high an annual runoff volume. Several other values were tried and it was found that 125% was a reasonable value

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APPENDIX A

Dictionary of Program Variables

<u>VARIABLE NAME</u>	<u>UNITS</u>	<u>DEFINITION</u>
ABFSL	DAY	ACCUMULATED BASE FLOW SEQUENCE LENGTH
ABFV	IN	ANNUAL BASE FLOW VOLUME
ACRFMI	-	ACCUMULATED CASES IN ALL RECORDED FLOOD MAGNITUDE INTERVALS
ADBF	IN	ACCUMULATED DAILY BASE FLOW
ADIF	IN	ACCUMULATED DAILY INTERFLOW
ADRSF	CFS	ACCUMULATED SUM OF DRSP
AETX	IN	ANNUAL EVAPOTRANSPIRATION INDEX
AEX90	IN	ANTECEDENT EVAPORATION INDEX, DECAY RATE = 0.9
AEX96	IN	ANTECEDENT EVAPORATION INDEX, DECAY RATE = 0.96
AFSIL	IN	ANNUAL FOREST SNOW INTERCEPTION LOSS
AHP	IN	ACCUMULATED HOURLY PRECIPITATION
AIFSL	DAY	ACCUMULATED INTERFLOW SEQUENCE LENGTH
AIFV	IN	ANNUAL INTERFLOW VOLUME
AMBER	IN	ANNUAL MOISTURE BALANCE ERROR
AMBF	IN	ACCUMULATED MONTHLY BASE FLOW
AMFSIL	IN	ACCUMULATED MONTHLY FOREST SNOW INTERCEPTION LOSS
AMIF	IN	ACCUMULATED MONTHLY INTERFLOW
AMNET	IN	ACCUMULATED MONTHLY NET EVAPOTRANSPIRATION
AMPET	IN	ACCUMULATED MONTHLY POTENTIAL EVAPOTRANSPIRATION
AMPREC	IN	ACCUMULATED MONTHLY PRECIPITATION
AMRPM	IN	ACCUMULATED MONTHLY RAIN PLUS MELT
AMRTF	CFS	ACCUMULATED MONTHLY RECORDED TOTAL FLOW

AMSE	IN	ACCUMULATED MONTHLY STREAM EVAPORATION
AMSNE	IN	ACCUMULATED MONTHLY SNOW EVAPORATION
AMSTF	CFS	ACCUMULATED MONTHLY SYNTHESIZED TOTAL FLOW
ANET	IN	ANNUAL NET EVAPOTRANSPIRATION
AOFV	IN	ANNUAL OVERLAND FLOW VOLUME
APET	IN	ANNUAL POTENTIAL EVAPOTRANSPIRATION
APPKP	-	ACCUMULATED PARAMETER PEAK PRODUCTS
APREC	IN	ANNUAL PRECIPITATION
AREA	SQ MI	AREA OF WATERSHED
ARHF	IN	ACCUMULATED ROUTED HYDROGRAPH FLOW
ARHPF	CFS	ACCUMULATED RECORDED HYDROGRAPH PEAK FLOWS
ARPM	IN	ANNUAL RAIN PLUS MELT
ARSTR	-	ACCUMULATED RATIO OF SYNTHESIZED TO RECORDED FLOWS
ASE	IN	ANNUAL SNOW EVAPORATION
ASEV	IN	ANNUAL STREAM EVAPORATION VOLUME
ASM	IN	ANNUAL SNOWFALL MOISTURE
ASMRG	IN	ANNUAL SNOWFALL MOISTURE REACHING GROUND
ASRR	CFS	ABSTRACTED SYNTHESIZED ROUTED RUNOFFS
ASRX	-	AVERAGE VALUE OF SRX
ATF	SFD	ACCUMULATED TOTAL FLOW
ATFV	SFD	ANNUAL TOTAL FLOW VOLUME
AVRHFP	CFS	AVERAGE VALUE OF RHFP
AWSBIT	-	ACCUMULATOR FOR WATERSHED BITS
BBMIR	IN/HR	CURRENT BEST ESTIMATE OF BASIC MAXIMUM INFILTRATION RATE

BBUZZ	-	CURRENT BEST ESTIMATE OF BASIC UPPER ZONE STORAGE CAPACITY FACTOR
BBYLZS	IN	CURRENT BEST ESTIMATE OF BEGINNING OF YEAR LOWER ZONE STORAGE
BDDFSM	IN/HR	BASIC DEGREE DAY FACTOR FOR SNOW MELT
BETLF	-	CURRENT BEST ESTIMATE OF EVAPOTRANSPIRATION LOSS FACTOR
BFHRC	-	BASE FLOW HOURLY RECESSON CONSTANT
BFNHR	-	BASE FLOW HOURLY NONLINEAR RECESSON ADJUSTMENT FACTOR
BFNLR	-	BASE FLOW NONLINEAR RECESSON ADJUSTMENT FACTOR
BFNRL	-	BASE FLOW NONLINEAR RECESSON LOGARITHM
BFNX	IN	CURRENT VALUE OF BASE FLOW NONLINEAR RECESSON INDEX
BFRG	-	BASE FLOW RECESSON CONSTANT
BFRL	-	BASE FLOW RECESSON LOGARITHM
BFSRX	-	CURRENT BEST ESTIMATE OF FSRX
BISRX	-	BIG INCREMENTAL STORAGE ROUTING INDEX
BIVF	-	BASIC INTERFLOW VOLUME FACTOR
BIZC	IN	CURRENT BEST ESTIMATE OF LOWER ZONE STORAGE CAPACITY
BMIR	IN/HR	BASIC MAXIMUM INFILTRATION RATE WITHIN WATERSHED
BSIAC	-	CURRENT BEST ESTIMATE OF SEASONAL INFILTRATION ADJUSTMENT FACTOR
BSUZZ	-	CURRENT BEST ESTIMATE OF SEASONAL UPPER ZONE STORAGE CAPACITY FACTOR
BTRI	-	BASE TIME ROUTING INCREMENTS
BUZC	-	BASIC UPPER ZONE STORAGE CAPACITY FACTOR
BYGWS	IN	BEGINNING OF YEAR GROUNDWATER STORAGE

BYIFS	IN	BEGINNING OF YEAR INTERFLOW STORAGE
BYLZS	IN	BEGINNING OF YEAR LOWER ZONE STORAGE
BYUZS	IN	BEGINNING OF YEAR UPPER ZONE STORAGE
CBF	IN/HR	CURRENT BASE FLOW
CCRFMI	-	CASES IN CURRENT RECORDED FLOW MAGNITUDE INTERVAL
CDSDR	-	CURRENT DAY FOR WHICH STORM DETAILS REQUESTED
CHBF	CFS	CURRENT HYDROGRAPH BASE FLOW
CHCAP	CFS	CHANNEL CAPACITY-INDEXED TO BASIN OUTLET
CHPV	-	CURRENT HYDROGRAPH PARAMETER VALUE
CIVM	-	CURRENT INTERFLOW VOLUME MULTIPLIER
CMIR	IN	CURRENT MAXIMUM INFILTRATION RATE DURING PERIOD
CN	-	1 = A.M., 2 = P.M.
CONOPT	-	CONTROL OPTION
CRFMI	-	CASES RECORDED IN FLOW MAGNITUDE INTERVAL
CRSBBF	CFS	CURRENT RECESSION SEQUENCE BEGINNING BASE FLOW
CRSBIF	CFS	CURRENT RECESSION SEQUENCE BEGINNING INTERFLOW
CRSBTF	CFS	CURRENT RECESSION SEQUENCE BEGINNING TOTAL FLOW
CRSTF	CFS	CURRENT RECESSION SEQUENCE TOTAL FLOWS
CRSOBF	CFS	CURRENT RECESSION SEQUENCE BASE FLOW ON DAY ZERO
CRSOIF	CFS	CURRENT RECESSION SEQUENCE INTERFLOW ON DAY ZERO
CSRX	-	CHANNEL STORAGE ROUTING INDEX
CTRI	-	CURRENT TIME ROUTING INCREMENTS
DATE	-	CURRENT DAY OF THE MONTH
DAY	-	CURRENT DAY OF THE YEAR
DBFRC	-	DOUBLE PRECISION BFRC

DDIW	CFS	DATED DIVERSIONS INTO WATERSHED
DFCC	-	DAILY FLOW CORRELATION COEFFICIENT
DIFRC	-	DOUBLE PRECISION IFRC
DIV	CFS	DIVERSION INTO BASIN, MEAN DAILY FLOW
DMNT	DEGF	DATED MINIMUM TEMPERATURE
DMXT	DEGF	DATED MAXIMUM TEMPERATURE
DNFS	-	DENSITY OF NEW FALLEN SNOW
DPET	IN	DATED POTENTIAL EVAPOTRANSPIRATION
DPSE	IN	DATED POTENTIAL SNOW EVAPORATION
DPY	-	DAYS PER YEAR
DRAF	CFS	DIFFERENCE BETWEEN RECORDED AND AVERAGE FLOW
DRGPM	-	DATED RECORDING GAGE PRECIPITATION MULTIPLIER
DRHP	IN	DATED RECORDED HOURLY PRECIPITATION
DRSF	CFS	DATED RECORDED STREAMFLOW
DRSGP	IN	DATED RECORDED STORAGE GAGE PRECIPITATION
DRSP	CFS	DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED HYDROGRAPH PEAKS
DSAF	CFS	DIFFERENCE BETWEEN SYNTHESIZED AND AVERAGE FLOW
DSMGH	IN	RATE OF DAILY SNOWMELT FROM GROUND HEAT
DSSF	CFS	DATED SYNTHESIZED STREAMFLOW
EDLZS	IN	END OF DAY VALUES OF LZS
EHSGD	-	ENDING HOUR OF STORAGE GAGE DAY
EHSGDF	-	ENDING HOUR OF STORAGE GAGE DAY-FLOATING POINT
EID	-	EXPONENT OF INFILTRATION RATE DECAY WITH INCREASED SOIL MOISTURE CONTENT

ELEVATION DIFFERENCE BETWEEN BASE THERMOMETER AND BASIN MEAN

ELDIF 1000ft

ELEVATION

ESTIMATED MAXIMUM ANNUAL EVAPOTRANSPIRATION

EMAET IN

END OF MONTH ACCUMULATED TOTAL FLOWS

EMATF SFD

END OF MONTH BASE FLOW NONLINEAR RECESSION INDEX

EMEFNX IN

EXTREME MONTHLY FLOW DEVIATION PARAMETER

EMFDP -

END OF MONTH GROUNDWATER STORAGE

ENGWS IN

END OF MONTH INTERFLOW STORAGE

EMIFS IN

END OF MONTH LOWER ZONE STORAGE

EMLZS IN

END OF MONTH SEASONAL INFILTRATION ADJUSTMENT MULTIPLIER

EMSIAM -

END OF MONTH UPPER ZONE STORAGE CAPACITY

ENUZC IN

END OF MONTH UPPER ZONE STORAGE

EMUZS IN

ESTIMATED POTENTIAL ANNUAL EVAPOTRANSPIRATION

EPAET IN

EVAPORATION PAN COEFFICIENT FOR MONTH

EPCM -

MAXIMUM REQUIRED ESTIMATING TOLERANCE

EPS -

EQUILIBRIUM DEPTH OF OVERLAND FLOW

EQD IN

EQUILIBRIUM DEPTH FACTOR FOR OVERLAND FLOW

EQDF -

EQUILIBRIUM DEPTH FACTOR FOR OVERLAND FLOW, IMPERVIOUS SURFACES

EQDFIS -

EQUILIBRIUM DEPTH OF OVERLAND FLOW IMPERVIOUS SURFACES

EQDIS IN

DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED DATED STREAMFLOW

ERR CFS

ERROR TABLE INTERVAL BOUNDARY FLOODS

ETIBF CFS

EVAPOTRANSPIRATION LOSS FACTOR

ETLTF -

EXPONENT OF FLOW PROPORTIONAL TO VELOCITY

EXQPV -

ADJUSTMENT FACTOR FOR BUZC

FBUZC -

FCNTRI	-	FLOATING POINT CHANGE IN NUMBER OF TIME ROUTING INCREMENTS
FDAY	-	FLOATING POINT CURRENT DAY OF THE YEAR
FDPY	-	FLOATING POINT DAYS PER YEAR
FDSC	-	FIRST DIFFERENTIAL OF SINE CURVE MAGNITUDE
FEELF	-	ADJUSTMENT FACTOR FOR ETLF
FFOR	-	FRACTION OF THE WATERSHED BEING FOREST
FFSI	-	FRACTION OF SNOW ON FOREST INTERCEPTED
FHPP	-	FRACTIONAL HOUR PER PERIOD
FIMP	-	FRACTION OF THE WATERSHED BEING IMPERVIOUS
FIRR	-	FRACTION OF INCOMING RADIATION REFLECTED BY SNOW SURFACE AS A FUNCTION OF AGE
FKRFMI	-	FLOATING POINT VALUE OF KRPMI
FLZC	-	ADJUSTMENT FACTOR FOR LZC
FMR	-	FRACTION OF MOISTURE RETENTION
FMXTRI	-	FLOATING POINT MAXIMUM NUMBER OF TIME ROUTING INCREMENTS
FNBTRI	-	FLOATING POINT NUMBER OF BASIC TIME ROUTING INCREMENTS
FNCTRH	-	FLOATING POINT NUMBER OF CURRENT TIME ROUTING HOURS
FNOFM	-	FLOATING POINT NUMBER OF OVERLAND FLOW MONTHS
FNPTRI	-	FLOATING POINT NUMBER OF PREVIOUS TIME ROUTING INCREMENTS
FNRHP	-	FLOATING POINT NUMBER OF RECORDED HYDROGRAPH PEAKS
FNSTRI	-	FLOATING POINT NUMBER OF SUBSEQUENT TIME ROUTING INCREMENTS
FNTRI	-	FLOATING POINT NUMBER OF TIME ROUTING INCREMENTS
FFPER	-	FRACTION OF THE WATERSHED BEING PERVIOUS
FRERS	CFS	FLOW RISE ENDING RECESSON SEQUENCE

FSIAC	-	ADJUSTMENT FACTOR FOR SIAC
FSIL	IN	HOURLY FOREST SNOW INTERCEPTION LOSS
FSRX	-	FLOOD PLAIN STORAGE ROUTING INDEX
FSUZC	-	ADJUSTMENT FACTOR FOR SUZC
FTA	-	FACTOR FOR ESTIMATING DIURNAL TEMPERATURE VARIATION BASED ON SINE CURVE
FTX	-	FALL TROUBLE INDEX
FWTR	-	FRACTION OF THE WATERSHED BEING WATER
GWET	IN	CURRENT HOURLY GROUNDWATER EVAPOTRANSPIRATION
GWETF	-	GROUNDWATER EVAPOTRANSPIRATION FACTOR
GWS	IN	CURRENT GROUNDWATER STORAGE
HBF	CFS	HYDROGRAPH BASE FLOW
HBEM	-	HYDROGRAPH BASE FLOW MULTIPLIER
HNTRI	-	HYDROGRAPH NUMBER OF TIME ROUTING INCREMENTS
HOUR	-	CURRENT HOUR OF THE DAY
HOURLF	HR	CURRENT HOUR OF THE DAY, FLOATING POINT
HRF	-	FIRST HOUR OF LOOP
HRL	-	LAST HOUR OF LOOP
HSE	IN	CURRENT HOURLY STREAM EVAPORATION
HSF	IN	HOURLY SNOWFALL
HSFRG	IN	HOURLY SNOWFALL REACHING GROUND
HSM	IN	HOURLY SNOWMELT RATE
HSRX	-	HYDROGRAPH STORAGE ROUTING INDEX
HTH	-	HOURS INTO DAY WHEN HYDROGRAPH STOPS OR STARTS
IBTPR	HR	TIME FROM BEGINNING OF SAVED RUNOFF TO RECORDED HYDROGRAPH

IBTFS	-	PEAK
	-	TIME FROM BEGINNING OF SAVED RUNOFF TO SYNTHESIZED HYDROGRAPH
	-	PEAK
IDAY1	-	INDEX TO 10-DAY PERIOD
IDAY2	-	INDEX WITHIN 10-DAY PERIOD
IDYB	-	DAY OF ROUTING HYDROGRAPH BEGINNING
IDYE	-	DAY OF ROUTING HYDROGRAPH ENDING
IFPRC	-	INTERFLOW PERIOD RECLSSION CONSTANT
IFRC	-	INTERFLOW RECLSSION CONSTANT
IFRL	-	INTERFLOW RECLSSION LOGARITHM
IFS	IN	INTERFLOW STORAGE
IFT	-	INDICATOR OF FILL TROUBLE
IHRB	-	HOUR OF DAY OF ROUTING HYDROGRAPH BEGINNING
IHRE	-	HOUR OF DAY OF ROUTING HYDROGRAPH ENDING
INHPT	HR	INTEGER NUMBER OF HOURS BETWEEN HYDROGRAPH PRINTING POINTS
IPPH	-	INTEGER PERIODS PER HOUR
IPTE	HR	TIME FROM PEAK OF RECORDED HYDROGRAPH TO END OF SAVED RUNOFF
ISGRD	-	CURRENT STORAGE GAGE RAINFALL DAY
IWBG	-	INDEX NUMBER OF WEATHER BUREAU PRECIPITATION GAGE
KAA	-	COUNTER OF APPROPRIATE ELEMENT FROM ALBEDO ARRAY
KAAB	-	PRECEDING VALUE OF KAA
KAPH	-	COUNTER FOR ABSTRACTED FLOW HYDROGRAPH
KAHP	-	COUNTER FOR ABSTRACTING HYDROGRAPH POINTS
KBRC	-	COUNTER OF ROUGH CYCLES SINCE BEST ONE

KB1-7
KDBCK
KDFOR
KDRS
KDY
KFPC
KHBCK
KHFOR
KHOUR
KHPN
KHYD
KH1-3
KIA
KISRX
KICGA
KMO
KM1-6
KPA
KPCH
KPRD
KPSH
KRC
KRD
KRFMI

COUNTERS FOR COMBINING WATERSHED BITS
BACKWARD DAY COUNTER
FORWARD DAY COUNTER
COUNTER OF CURRENT DAY IN RECESSIOIN SEQUENCE
COUNTER FOR DAY
COUNTER EQUALLING ONE ON FIRST FINE ADJUSTMENT CYCLE
BACKWARD HOUR COUNTER
FORWARD HOUR COUNTER
COUNTER FOR HOUR OF DAY
COUNTER OF CURRENT HYDROGRAPH POINT
COUNTER SPECIFYING CURRENT HYDROGRAPH
COUNTERS FOR FIXING HYDROGRAPH ROUTING PARAMETERS
COUNTER FOR INITIALIZING ARRAYS
COUNTER FOR INCREMENTING STORAGE ROUTING INDEX
COUNTER FOR LIMITING NUMBER OF CHANNEL CAPACITY ADJUSTMENTS
COUNTER INDEXING MONTH OF THE YEAR
MONTH COUNTERS
COUNTER DESIGNATING PARAMETER TO BE AVERAGED
COUNLED POINTS IN CURRENT HYDROGRAPH
COUNTER FOR PERIOD
COUNTER POINTS IN SUBSCRIPTED HYDROGRAPH
COUNTER OF CURRENT ROUGH CYCLE
COUNTER FOR READING DATA ARRAYS
COUNTER FOR RECORDED FLOW MAGNITUDE INTERVAL

KRHP	-	COUNTER FOR RECORDED HYDROGRAPH PEAKS
KRIA	-	COUNTER OF APPROPRIATE ELEMENT FROM RADIATION INCIDENCE ARRAY
KRS	-	COUNTER FOR RECESSION SEQUENCE NUMBER
KSD	-	COUNTER FOR RECESSION SEQUENCE DAYS
KSQ	-	COUNTER FOR REVISED SEQUENCES
KTA	-	COUNTER FOR TITLE ARRAY
KTRI	-	COUNTER FOR TIME ROUTING INCREMENTS
KT20	-	COUNTER FOR TOP 20 VALUES
KWD	-	COUNTER FOR WRITING DATA ARRAYS
KWSM	-	COUNTER OF WEST SUMMER MONTHS
KLAH	-	COUNTER FOR FIRST ACCEPTED HYDROGRAPH
K24H	-	COUNTER FOR SECOND ACCEPTED HYDROGRAPH
LBFO	-	LOGICAL VARIABLE SET TRUE WHERE BASE FLOW ONLY ENCOUNTERED
LBMIR	-	LOGICAL VARIABLE SET TRUE WHEN EXERCISING SUBSTITUTE APPROACH FOR EVALUATING BMIR
LBUCZ	-	LOGICAL VARIABLE SET TRUE WHEN EXERCISING SUBSTITUTE APPROACH FOR EVALUATING BUZC
LDAY	-	LAST DAY OF YEAR
LHOUR	-	LAST HOUR OF DAY
LLZC	-	LOGICAL VARIABLE SET TRUE WHEN EXERCISING SUBSTITUTE APPROACH FOR EVALUATING LZC
LNIBRS	-	LAST VALUE OF NIBRS
LNPR	-	LOGICAL VARIABLE SET TRUE FOR NONEQUAL PERIOD RAINFALL

LNTRI	-	LAST NUMBER OF TIME ROUTING INCREMENTS
LRC	-	LOGICAL VARIABLE SET TRUE DURING ROUGH ADJUSTMENT CYCLES
LSHA	-	LOGICAL VARIABLE KEPT TRUE WHILE SYNTHESIZED HYDROGRAPH IS ACCEPTED FOR COMPARISON WITH RECORDED HYDROGRAPH
LSHFT	-	LOGICAL VARIABLE SET TRUE WHILE SHIFTING THE NUMBER OF TIME ROUTING INCREMENTS
LSHP	-	LOGICAL VARIABLE SET TRUE DURING STORM HYDROGRAPH PERIODS
LZC	IN	LOWER ZONE STORAGE CAPACITY
LZRX	-	LOWER ZONE MOISTURE RETENTION INDEX
LZS	IN	CURRENT LOWER ZONE STORAGE
LZSR	-	CURRENT LOWER ZONE STORAGE RATIO (LZS/LZC)
MBDS	-	MONTH BEGINNING DRY SEASON
MBWS	-	MONTH BEGINNING WET SEASON
MDAY	-	DAY OF YEAR OF LAST DAY OF PREVIOUS MONTH
MEDCY	-	MONTH END DATES--CALENDAR YEAR
MEDWY	-	MONTH END DATES-WATER YEAR
MFDP	-	MONTHLY FLOW DEVIATION PARAMETER
MHSM	IN	MINIMUM HOURLY SNOWMELT RATE
MHTP	-	MULTIPLIER CONVERTING FROM HOURS TO PERIODS
MNDRS	-	MAXIMUM NUMBER OF DAYS IN RECESSION SEQUENCE
MNRC	-	MINIMUM NUMBER OF ROUGH CYCLES
MNRD	-	MEAN ANNUAL NUMBER OF RAINY DAYS
MNTRI	-	MINIMUM NUMBER OF TIME ROUTING INCREMENTS
MNX	-	MONTH INDEX

MONTH	-	CURRENT MONTH OF THE YEAR
MONTH1	-	COUNTER FOR BEGINNING MONTH
MRNSM	IN	MAXIMUM RATE OF NEGATIVE SNOWMELT (SNOW CHILLING)
MRS1	DAY	MINIMUM RECESSON SEQUENCE LENGTH
MXA	-	MONTH INDEX ARRAY
MXTRH	-	MAXIMUM NUMBER OF TIME ROUTING HOURS
MXTRI	-	MAXIMUM NUMBER OF TIME ROUTING INCREMENTS
M1R	-	MONTH WITH MOST RUNOFF
M1SP	-	MONTH WITH MOST SUMMER PRECIPITATION
M11	-	SET AT 11 IF AUGUST IS A BASE FLOW MONTH
M12	-	SET AT 12 IF SEPTEMBER IS A BASE FLOW MONTH
M2R	-	MONTH WITH SECOND MOST RUNOFF
M2SP	-	MONTH WITH SECOND MOST SUMMER PRECIPITATION
NATR	-	NUMBER OF ANTICIPATED TIME ROUTING HOURS
NBTRI	-	NUMBER OF BASE TIME ROUTING INCREMENTS
NCSTRI	-	NUMBER OF CURRENT TIME ROUTING INCREMENTS DURING SHIFTING
NCTRH	-	NUMBER OF CURRENT TIME ROUTING HOURS
NCTRI	-	NUMBER OF CURRENT TIME ROUTING INCREMENTS
NDAY	-	NEXT DAY OF YEAR
NDRS	DAY	NUMBER OF DAYS IN RECESSON SEQUENCE
NDRSC	DAY	NUMBER OF DAYS IN CURRENT RECESSON SEQUENCE
NDRSC1	DAY	NUMBER OF DAYS IN CURRENT RECESSON SEQUENCE LESS 1
NDRSC2	DAY	NUMBER OF DAYS IN CURRENT RECESSON SEQUENCE LESS 2
NDSDP	DAY	NUMBER OF DAYS FOR WHICH STORM DETAILS HAVE ALREADY BEEN

PRINTED

NDSDR	DAY	NUMBER OF DAYS FOR WHICH STORM DETAILS REQUESTED
NFRHA	-	NUMBER OF FIRST RAINFALL HOUR ADJUSTED, PREVIOUS DAY
NFTR	-	NUMBER OF FIRST TRIP TO BE RUN FOR A GIVEN STATION YEAR
NHOUR	-	NEXT HOUR OF DAY
NHPT	HR	NUMBER OF HOURS BETWEEN HYDROGRAPH PRINTING POINTS
NIBRS	-	NUMBER OF TIME ROUTING INTERVALS BETWEEN RECORDED AND SYNTHESIZED PEAKS
NIRTS	-	NUMBER OF TIME ROUTING INTERVALS FROM RECORDED TO SYNTHESIZED PEAK
NLTR	-	NUMBER OF LAST TRIP TO BE RUN FOR A GIVEN STATION YEAR
NNSTRI	-	NUMBER OF NEXT TIME ROUTING INCREMENT DURING SHIFTING
NOFM	-	NUMBER OF OVERLAND FLOW MONTHS
NORHP	-	NUMBER OF ORIGINAL RECORDED HYDROGRAPH PEAKS
NOYR	YEAR	NUMBER OF YEAR TO BE SIMULATED
NRHA	-	NUMBER OF RAINFALL HOURS ADJUSTED, CURRENT DAY
NRHP	-	NUMBER OF RECORDED HYDROGRAPH PEAKS
NRHPI	-	NUMBER OF RECORDED HYDROGRAPH PEAKS LESS ONE
NRS	-	NUMBER OF RECESSION SEQUENCES
NRTRI	-	NUMBER OF TIME ROUTING INCREMENTS REMAINING TO BE ROUTED
NSGRD	-	NUMBER OF STORAGE GAGE RAINFALL DAYS
NSYC	-	NUMBER OF STATION YEAR, CURRENT ONE BEING RUN
NSYT	-	NUMBER OF STATION YEARS, TOTAL INCLUDED IN A GIVEN JOB
NTRS	-	NUMBER OF TENTATIVE RECESSION SEQUENCES

OCT1BF	-	OCTOBER FIRST BASE FLOW
OFMN	-	OVERLAND FLOW MANNING'S N
OFMNIS	-	OVERLAND FLOW MANNING'S N, IMPERVIOUS SURFACES
OFR	IN	CURRENT OVERLAND FLOW RUNOFF
OFRF	-	OVERLAND FLOW ROUTING FACTOR
OFRFIS	-	OVERLAND FLOW ROUTING FACTOR, IMPERVIOUS SURFACES
OFRIS	IN	CURRENT OVERLAND FLOW RUNOFF, IMPERVIOUS SURFACES
OFS	IN	OVERLAND FLOW STORAGE
OFSL	FT	OVERLAND FLOW SURFACE LENGTH
OFSS	-	OVERLAND FLOW SURFACE SLOPE
OFUS	IN	CURRENT OVERLAND FLOW UNROUTED STORAGE
OFUSIS	IN	CURRENT OVERLAND FLOW UNROUTED STORAGE, IMPERVIOUS SURFACES
PBIVF	-	PERVIOUS VALUE OF BIVF
PBMIR	IN/HR	PREVIOUS VALUE OF BMR
PBUZC	-	PREVIOUS ESTIMATE OF BASIC UPPER ZONE STORAGE CAPACITY FACTOR
PDAY	-	PREVIOUS DAY OF THE YEAR
PEAI	IN	PRECIPITATION EXCESS AFTER INFILTRATION
PEBI	IN	PRECIPITATION EXCESS, BEFORE INFILTRATION
PEIS	IN	PRECIPITATION EXCESS ON IMPERVIOUS SURFACES
PEP	IN	PRECIPITATION ESTIMATED FOR PERIOD
PET	IN	CURRENT DAILY POTENTIAL EVAPOTRANSPIRATION
PETLF	-	PREVIOUS ESTIMATE OF EVAPOTRANSPIRATION LOSS FACTOR
PETU	IN	UNADJUSTED CURRENT DAILY POTENTIAL EVAPOTRANSPIRATION

PE4P	IN	PRECIPITATION ESTIMATES FOR 4 PERIODS
PGW	IN	PERCOLATION TO GROUND WATER
PLZC	IN	PREVIOUS ESTIMATE OF LZC STORAGE
PLZS	IN	PERCOLATION TO LOWER ZONE STORAGE
PMEIFS	IN	PERIOD MOISTURE ENTERING INTERFLOW STORAGE
PMELZS	IN	PERIOD MOISTURE ENTERING LOWER ZONE STORAGE
PMEOFS	IN	PERIOD MOISTURE ENTERING OVERLAND FLOW STORAGE
PMEUFS	IN	PERIOD MOISTURE ENTERING UPPER ZONE STORAGE
PPH	-	PERIODS PER HOUR
PPI	IN	PRECIPITATION PASSING INTERCEPTION
PRD	-	CURRENT PERIOD OF THE HOUR
PRDF	-	CURRENT PERIOD OF THE HOUR-FLOATING POINT
PRH	IN	PRECIPITATION RECORDED FOR HOUR
PRLH	IN	PRECIPITATION RECORDED FOR LAST HOUR
PRM1	IN	PRECIPITATION DURING WETTEST MONTH
PRM2	IN	PRECIPITATION DURING SECOND WETTEST MONTH
PRNH	IN	PRECIPITATION RECORDED FOR NEXT HOUR
PSIAC	-	PREVIOUS ESTIMATE OF SEASONAL INFILTRATION ADJUSTMENT
PSUZC	-	PREVIOUS ESTIMATE OF SEASONAL UPPER ZONE STORAGE CAPACITY FACTOR
PXCSA	IN	PRECIPITATION INDEX FOR CHANGING SNOW ALBEDO
RA	-	RECESSION ALPHA
RAA	IN	RAINFALL ADJUSTMENT ADDITION
RADF	CFS	RECORDED AVERAGE DAILY FLOW

RAM	-	RAINFALL ADJUSTMENT MULTIPLIER
RATFV	SFD	RECORDED ANNUAL TOTAL FLOW VOLUME
RA1-6	-	REGRESSION ACCUMULATORS
RB	-	RECESSION BETA
RBF	CFS	RECORDED BASE FLOW
RD	-	RECESSION DISCRIMINANT
RDPT	IN	RECORDED DAILY PRECIPITATION TOTAL
RFRISE	IN	RECORDED FLOW RISE
RGPM	-	RECORDING GAGE PRECIPITATION MULTIPLIER
RGPMB	-	RECORDING GAGE PRECIPITATION MULTIPLIER - BASIC
RHFMC	IN	ROUTED HYDROGRAPH FLOW AT MINIMUM CUTOFF
RHFO	IN	PRECEDING ROUTED HYDROGRAPH FLOW
RHF1	IN	CURRENT ROUTED HYDROGRAPH FLOW (EXCLUDING BASE FLOW)
RHPD	-	RECORDED HYDROGRAPH PEAK DAY
RHPF	CFS	RECORDED HYDROGRAPH PEAK FLOW
RHPH	-	RECORDED HYDROGRAPH PEAK HOUR
RICD	-	RADIATION INCIDENCE FOR THE CURRENT DAY
RICY	-	RADIATION INCIDENCE OVER THE CALENDAR YEAR
RIF	CFS	RECORDED INTERFLOW
RINT	-	REGRESSION INTERCEPT
RMFV	-	RECORDED MONTHLY FLOW INDEX
RMPF	CFS	REQUESTED MINIMUM DAILY PEAK FLOW TO BE PRINTED
RMWR	IN	RAINFALL MAXIMUM WITHOUT RUNOFF
RSBBF	CFS	ESTIMATED BASE FLOW AT BEGINNING OF RECESSION SEQUENCE

RSBD	-	RECESSION SEQUENCE BEGINNING DAY
RSBFRG	-	RECESSION SEQUENCE BASE FLOW RECESSION CONSTANT
RSBIF	CFS	ESTIMATED INTERFLOW AT BEGINNING OF RECESSION SEQUENCE
RSFM	CFS	RECESSION SEQUENCE FLOW MINIMUM
RSFN	CFS	RECORDED STREAMFLOW ON NEW DAY
RSF1	CFS	RECORDED STREAMFLOW ON DAY 1
RSF2	CFS	RECORDED STREAMFLOW ON DAY 2
RSIFRC	-	RECESSION SEQUENCE INTERFLOW RECESSION CONSTANT
RSL	DAY	CURRENT RECESSION SEQUENCE LENGTH
RSIF	-	REGRESSION SLOPE
RSPTF	IN	ROUTED SYNTHESIZED PERIOD TOTAL FLOW
RSTF	CFS	RECESSION SEQUENCE TOTAL FLOWS
RSTR	-	RATIO OF SYNTHESIZED TO RECORDED FLOW
RWRAIN	IN	RECORDED WATERSHED RAINFALL
SADF	CFS	SYNTHESIZED AVERAGE DAILY FLOW
SARAX	IN	SNOW ALBEDO RAINFALL AGING INDEX
SASFX	IN	SNOW ALBEDO SNOWFALL FRESHENING INDEX
SATFV	SFD	SYNTHESIZED ANNUAL TOTAL FLOW VOLUME
SATFVI	IN	SYNTHESIZED ANNUAL TOTAL FLOW VOLUME IN INCHES
SATRI	-	SHIFT ADJUSTMENTS FOR TIME ROUTING INCREMENTS
SAX	-	SNOW ALBEDO INDEX
SBF	CFS	SYNTHESIZED BASE FLOW
SBFRS	CFS	SYNTHESIZED BASE FLOW DURING THE FIRST THREE DAYS OF EACH RECESSION SEQUENCE

SDEPTH	IN	AVERAGE DEPTH OF SNOW ON GROUND
SDRSP	-	SMALLEST VALUE OF DRSP
SDSC	-	SECOND DIFFERENTIAL OF SINE CURVE MAGNITUDE
SE	IN	CURRENT DAILY SNOW EVAPORATION
SERA	CFS	ACCUMULATED ABSOLUTE DIFFERENCES BETWEEN RECORDED AND SYNTHESIZED DAILY STREAMFLOWS FOR INTERVAL
SERAV	CFS	AVERAGE INTERVAL ABSOLUTE DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED DAILY STREAMFLOWS
SERR	CFS	ACCUMULATED DIFFERENCES BETWEEN RECORDED AND SYNTHESIZED DAILY STREAMFLOWS FOR INTERVAL
SERRV	CFS	AVERAGE INTERVAL DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED DAILY STREAMFLOWS
SESF	CFS	STANDARD ERROR OF SYNTHESIZED FLOWS BY MAGNITUDE INTERVAL
SET	IN	CURRENT HOURLY SOIL EVAPOTRANSPIRATION
SFDX	-	SUMMER FLOW DEVIATION INDEX
SFMD	-	SNOW FROZEN MOISTURE DENSITY
SGMD	-	STORAGE GAGE MOVING DAY (WHEN IT IS MOVED DURING WATER YEAR)
SGRT	-	STORAGE GAGE READING TIME
SGRT2	-	SECOND STORAGE GAGE READING TIME
SHM	-	SYNTHESIZED HYDROGRAPH MULTIPLIER
SHPF	CFS	SYNTHESIZED HYDROGRAPH PEAK FLOW
SIAC	-	SEASONAL INFILTRATION ADJUSTMENT CONSTANT
SIAM	-	SEASONAL INFILTRATION ADJUSTMENT MULTIPLIER

SIF	CFS	SYNTHESIZED INTERFLOW
SIFRS	CFS	SYNTHESIZED INTERFLOW DURING THE FIRST THREE DAYS OF EACH RECESSION SEQUENCE
SISRX	-	SMALL INCREMENTAL STORAGE ROUTING INDEX
SMFX	-	SYNTHESIZED MONTHLY FLOW INDEX
SNTRI	-	SAVED NUMBER OF TIME ROUTING INCREMENTS
SOFMD	-	SUM OF OVERLAND FLOW MONTH DEVIATIONS
SOFRF	-	SNOW OVERLAND FLOW ROUTING FACTOR
SOFRFI	-	SNOW OVERLAND FLOW ROUTING FACTOR IMPERVIOUS SURFACES
SPBF	IN	SYNTHESIZED PERIOD BASE FLOW
SPBFLW	-	SNOW PACK BASIC MAXIMUM FRACTION IN LIQUID WATER
SPDR	IN	SYNTHESIZED PERIOD DIRECT RUNOFF
SPIF	IN	SYNTHESIZED PERIOD INTERFLOW
SPLW	IN	SNOW PACK LIQUID WATER CONTENT
SPLWC	IN	SNOWPACK LIQUID WATER HOLDING CAPACITY
SPM	-	SNOW PRECIPITATION MULTIPLIER
SPOF	CFS	SYNTHESIZED PERIOD OVERLAND FLOW (INCLUDING CHANNEL PRECIPITATION)
SPTF	IN	SYNTHESIZED PERIOD TOTAL FLOW
SPTW	IN	SNOW PACK TOTAL WATER CONTENT
SPTWCC	IN	SNOWPACK MINIMUM TOTAL WATER FOR COMPLETE BASIN COVERAGE
SQER	CFS	ACCUMULATED SQUARES OF DIFFERENCES BETWEEN RECORDED AND SYNTHESIZED DAILY STREAMFLOWS
SQPKD	-	SUM OF SQUARED PEAK DIFFERENCES
SRR	CFS	STORM RUNOFF ROUTED DOWN CHANNELS

SRX	-	CURRENT STORAGE ROUTING INDEX
SSERA	CFS	ACCUMULATED ABSOLUTE DIFFERENCES BETWEEN RECORDED AND SYNTHESIZED FLOWS OVER INTERVALS
SSERAV	CFS	OVERALL AVERAGE ABSOLUTE DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED FLOWS
SSERR	CFS	ACCUMULATED DIFFERENCES BETWEEN RECORDED AND SYNTHESIZED FLOWS OVER INTERVALS
SSERRV	CFS	OVERALL AVERAGE DIFFERENCE BETWEEN RECORDED AND SYNTHESIZED FLOWS
SSESF	CFS	ACCUMULATED STANDARD ERROR OF SYNTHESIZED FLOW OVER INTERVALS
SSQM	-	SUM OF THE SQUARES OF THE MONTHLY FLOW DEVIATIONS
SSQPKD	-	SMALLEST VALUE OF SQPKD
SSR	CFS	SYNTHESIZED STORM RUNOFF (NOT CHANNEL ROUTED)
SSRT	-	SQUARE ROOT OF OVERLAND FLOW SURFACE SLOPE
SSSQM	-	CURRENT SMALLEST ESTIMATE OF SSQM
STMD	-	SNOW TOTAL MOISTURE DENSITY
SUBWF	-	SUBSURFACE WATER FLOW OUT OF THE BASIN
SUZC	-	SEASONAL UPPER ZONE STORAGE CAPACITY FACTOR
SWSMD	-	SUM OF WET SUMMER MONTH DEVIATIONS
TANSM	IN	TOTAL ACCUMULATED NEGATIVE SNOWMELT (SNOW CHILLING)
TBRD	-	TOTAL BASE FLOW RECESSION DAYS
TDFP12	-	TIME OF DAILY FLOOD PEAK, 12-HOUR CLOCK
TDFP24	-	TIME OF DAILY FLOOD PEAK, 24-HOUR CLOCK

TDSF	CFS	TOTAL DAILY STREAMFLOW
TEH	DEGF	TEMPERATURE ESTIMATED FOR HOUR
TFCFS	CFS	CURRENT TOTAL FLOW
TFMAX	CFS	MAXIMUM TOTAL FLOW DURING CURRENT DAY
TFMRT	CFS	TOTAL STREAMFLOW AT MAXIMUM STREAM ROUTING TIME
TFSRX	-	TRIAL VALUE OF FSRX
TFX	CFS	TOTAL STREAMFLOW INDEX
THGR	IN/HR	TOTAL HOURLY GROSS RUNOFF
THSF	CFS	TOTAL HOURLY STREAMFLOW
TIRD	-	TOTAL INTERFLOW RECESSON DAYS
TITLE	-	TITLE OF CURRENT STATION YEAR
TMBF	IN	TOTALS OF MONTHLY BASE FLOW
TMFSIL	IN	TOTALS OF MONTHLY FOREST SNOW INTERCEPTION LOSS
TMIF	IN	TOTALS OF MONTHLY INTERFLOW
TMNET	IN	TOTALS OF MONTHLY NET EVAPOTRANSPIRATION
TMOF	IN	TOTALS OF MONTHLY OVERLAND FLOW
TMPET	IN	TOTALS OF MONTHLY POTENTIAL EVAPOTRANSPIRATION
TMPREC	IN	TOTALS OF MONTHLY PRECIPITATION
TMRPM	IN	TOTALS OF MONTHLY RAIN PLUS MELT
TMRTF	SFD	TOTALS OF MONTHLY RECORDED TOTAL FLOW
TMSE	IN	TOTALS OF MONTHLY STREAM EVAPORATION
TMSNE	IN	TOTALS OF MONTHLY SNOW EVAPORATION
TMSTF	SFD	TOTALS OF MONTHLY SYNTHESIZED TOTAL FLOW

TMSTFI	IN	TOTALS OF MONTHLY SYNTHESIZED TOTAL FLOW IN INCHES
TMSTFY	SFD	TOTALS OF MONTHLY TOTAL FLOW BY CALENDAR YEAR
TMSTWY	SFD	TOTALS OF MONTHLY TOTAL FLOW BY WATER YEAR
TOPR	IN	CURRENT TOTAL OVERLAND FLOW RUNOFF
TPLR	-	TOTAL TO PERVIOUS LAND RATIO
TRHF	IN/HR	CURRENT TIME ROUTED HYDROGRAPH FLOW
TRHV	-	TOTAL RECORDED HYDROGRAPH VOLUME
TRIP	-	COUNTER SPECIFYING PROGRAM PORTIONS
TSHV	-	TOTAL SYNTHESIZED HYDROGRAPH VOLUME
TSRX	-	ARRAY OF TRIAL STORAGE ROUTING INDICES
T20OFH	IN	TOP 20 VALUES DURING THE YEAR OF HOURLY OVERLAND FLOW
T20PRH	IN	TOP 20 VALUES DURING THE YEAR OF HOURLY PRECIPITATION
UHFA	IN	UNROUTED HYDROGRAPH FLOW ARRAY
URHF	IN	CURRENT UNROUTED HYDROGRAPH FLOW
UZC	IN	UPPER ZONE STORAGE CAPACITY
UZINFX	-	UPPER ZONE INFILTRATION INDEX
UZINLZ	IN/HR	CURRENT UPPER ZONE INFILTRATION TO LOWER ZONE
UZRX	-	UPPER ZONE MOISTURE RETENTION INDEX
UZS	IN	CURRENT UPPER ZONE STORAGE
VDCY	-	VALUE DATED BY CALENDAR DAY
VDMD	-	VALUE DATED BY MONTH DAY
VINTCR	IN	VEGETATIVE INTERCEPTION - CURRENT RATE PER PERIOD
VINTMR	IN/HR	VEGETATIVE INTERCEPTION - MAXIMUM RATE
VWIN	SFD	VOLUME OF AN INCH OF RUNOFF FROM WATERSHED

WAPV	-	WEIGHTED AVERAGE PARAMETER VALUE
WCFS	CFS	WATERSHED CFS EQUALLING ONE INCH PER HOUR
WEIFS	IN	WATER ENTERING INTERFLOW STORAGE
WFDX	-	WINTER FLOW DEVIATION INDEX
WI	IN	WATER INFILTRATION
WSBIT	-	WATERSHED BIT FOR RESTRUCTURING TIME--AREA HISTOGRAM
WSG	-	WEIGHTING FACTOR FOR STORAGE RAIN GAGE
WSG2	-	SECOND WEIGHTING FACTOR FOR STORAGE RAIN GAGE
WSM	-	NUMBER OF WET SUMMER MONTHS
WT4AM	DEGF	AVERAGE 4 A.M. TEMPERATURE OVER WATERSHED
WT4PM	DEGF	AVERAGE 4 P.M. TEMPERATURE OVER WATERSHED
XDNFS	-	INDEX DENSITY OF NEW-FALLEN SNOW
XEIR	-	RAIN INDEX FOR ESTIMATING LAPSE RATE 0.0=DRY, 4.0=RAIN
XMPFT	-	INDEX OF MONTHLY PREDOMINATE FLOW TYPE
YEAR	-	LAST TWO DIGITS OF CURRENT YEAR
YR1	-	LAST TWO DIGITS OF FIRST CALENDAR YEAR IN WATER YEAR
YR2	-	LAST TWO DIGITS OF SECOND CALENDAR YEAR IN WATER YEAR
YTITLE	-	YEAR TITLE

APPENDIX B

Computer Program

THIS PROGRAM IS BASED ON THE KENTUCKY VERSION OF THE STANFORD WATERSHED MODEL. PROGRAM JUSTIFICATIONS HAVE BEEN MADE AS STATED BELOW TO OPERATE ON THE IBM 360/40 DIGITAL COMPUTER:

- (1) READ SUBROUTINE HAS BEEN CHANGED INTO CONVENTIONAL READ STATEMENT ALONG WITH THE INPUT DATA FORMAT.
- (2) EVPDAY SUBROUTINE HAS BEEN TAKEN OUT WITHJUT ANY INTERFERENCE WITH THE MAIN PROGRAM.
- (3) ADDITIONAL CONTROL WAS ADDED TO TERMINATE THE PROGRAM.
- (4) MORE COMMENT STATEMENTS BEEN ADDED.
- (5) ADDITIONAL OPTION CODE PRINT OUT.

MAIN0001
MAIN0002

KENTUCKY WATERSHED MODEL (VERSION OF JUNE 6, 1970)
BASED ON STANFORD WATERSHED MODELS III & IV

```

DIMENSION BTRI(99), CONOPT(15), CRFXI(22), CTP I(99), DDIV(366),
1 DMNT(366), DMXT(366), DPSE(366), DRGPM(366), DRHP(366,24),
2 DRSGP(366), DPET(366), DRSF(366), DSSF(366), EDLZS(366),
3 EMBFNX(12), EMGX(12), EMIFS(12), EMLZS(12), EMSIAM(12),
4 EMUZC(12), EMUZS(12), EPCM(12), FIRR(15), MEDCY(12), MEDWY(12),
5 RICY(37), SATRI(99), SERA(22), SERR(22), SESF(22), SQER(22),
6 THSF(24), TTITLE(20), TMBF(12), TMFSIL(12), TMIF(12), TMNET(12),
7 TMOF(12), TMPET(12), TMPREC(12), TMRPM(12), TMRIF(12), TMSE(12),
8 TMSNE(12), TMSTF(12), TMSTFI(12), T20OFH(21), T20PRH(21),
9 UHFA(99), YTTITLE(20)
LOGICAL LSHFT
INTEGER CDSDR,CN,CONOPT,DATE,DAY,DPY,EHSGD,HOUR,HRF,HRL,PDAY,
1 PRD,RHPD,RHPH,RSBD,SGMD,SGRT,SGRT2,YEAR,YR1,YR2
REAL IFPRC,IFRC,IFRL,IFS,31,59,90,120,151,181,212,243,273,304,334/
DATA MEDCY/ 0,
DATA MEDWY/304,334,365,31,59,90,120,151,181,212,243,273 /

```

MAIN0003
MAIN0004
MAIN0005
MAIN0006
MAIN0007
MAIN0008
MAIN0009
MAIN0010
MAIN0011
MAIN0012
MAIN0013
MAIN0014
MAIN0015
MAIN0016
MAIN0017
MAIN0018

C PEAD IN NUMBER OF YEARS OF INPUT DATA REQUIRED.

IDAHO001
IDAHO002
MAIN0019

READ(5,2050)NOYR
2050 FORMAT(I2)
100 CONTINUE

C CONTROL OPTIONS (BALANCE OF DATA VARIES WITH SPECIFIED OPTIONS).

IDAHO003
IDAHO004
IDAHO005
IDAHO006
IDAHO007
IDAHO008
MAIN0022
MAIN0023
MAIN0024
MAIN0025
MAIN0026

DO 101 KRD=1,14
101 READ(5,2000) CONOPT(KRD)
2000 FORMAT(I2)
WRITE(6,997)
997 FORMAT('1')
WRITE(6,998)
998 FCRMAT('1',45X,'CONTROL OPTION CODE TABLE')
DO 99 J=1,14
99 WRITE(6,999) CONOPT(J),J
999 FCRMAT(/50X,'*',I2,' * OPTION ',I2,' *')
DO 102 KIA = 1,99
SATRI(KIA) = 0.0
CTRI(KIA)=0.0
BTRI(KIA) = 0.0
UHFA(KIA)=0.0
102 READ(5,2001) NCTRI
2001 FORMAT(I3)
READ(5,2002) (CTRI(KRD),KRD=1,NCTRI)
2002 FORMAT(10F7.5)
IF(CONOPT(7) .NE. 1) GO TO 110
READ(5,2003)(FIRR(KRD),KRD=1,15)
2003 FORMAT(15F5.3)

MAIN0030
MAIN0031

C READ IN RADIATION INCIDENCE OVER CALENDAR YEAR.

MAIN0033

READ(5,2004)(RICY(KRD),KRD=1,37)
2004 FORMAT(10F5.3)

C READ IN DATED POTENTIAL SNOW EVAPORATION DATA OVER WATER YEAR.

MAIN0035
MAIN0037
MAIN0039
MAIN0040
MAIN0041
MAIN0042
MAIN0043
MAIN0044
MAIN0045
MAIN0046
MAIN0047
MAIN0048
MAIN0049
MAIN0050

```

C
C
C   READ(5,2005)(DPSE(KRD),KRD=274,360,10)
C   FORMAT(9F7.5)
C   READ(5,2006)(DPSE(KRD),KRD=1,273,10)
C   FCFORMAT(10F7.5)
C   DO 109 IDAY2 = 1, 9
C   DO 108 IDAY1 = 274,360,10
C   DAY = IDAY1 + IDAY2
C   108 DPSE(DAY) = DPSE(IDAY1)
C   DO 109 IDAY1 = 1,273,10
C   DAY = ICAY1 + IDAY2
C   IF(DAY.GT. 273) GO TO 109
C   DPSE(DAY) = DPSE(IDAY1)
C   109 CONTINUE
C   DPSE(366) = DPSE(59)
C   DPSE(365) = DPSE(363)
C   DPSE(364) = DPSE(363)

```

C READ IN SNOWMELT PARAMETERS.
C
C READ(5,2007)BDDFSM, SPBFLW, SPTWCC, SPM, ELDIF, XDNFS, FFOR, FFSI

```

C   2007 FORMAT(8F10.0)
C   READ(5,3007)MRNSM,DSMGMH,PXCSEA
C   3007 FORMAT(3F10.7)
C   110 READ(5,2008) RMPF
C   2008 FORMAT(F10.0)

```

C READ IN WATERSHED PARAMETERS.
C
C READ(5,2009) RGPMB,AREA,FIMP,FWTR
C 2009 FORMAT(4F10.4)

C READ IN SOIL MOISTURE PARAMETERS.
C
C READ(5,2010) VINTMR,BUZZC,SUZZC,LZC,ETLF,SUBWF,GWETF,SIAC,BMIR,BIVF
C 2010 FORMAT(10F8.6)

MAIN0081
 MAIN0082
 MAIN0083
 MAIN0084
 MAIN0085
 MAIN0086
 MAIN0087
 MAIN0088
 MAIN0089
 MAIN0090
 MAIN0091
 MAIN0092
 MAIN0093
 MAIN0094
 MAIN0095
 MAIN0096
 MAIN0097
 MAIN0098
 MAIN0099
 MAIN0100
 MAIN0101
 MAIN0102
 MAIN0103
 MAIN0104
 MAIN0105
 MAIN0106
 MAIN0107
 MAIN0108
 MAIN0109
 MAIN0110
 MAIN0111
 MAIN0112
 MAIN0113
 MAIN0114
 MAIN0115
 MAIN0116
 MAIN0117

```

FPER = 1.0 - FIMP - FWTR
IF(FPER .GT. 0.01) GO TO 114
TPLR = 100.0
FPER = 0.01
GO TO 115
114 TPLR = (1.0 - FWTR)/FPER
115 VINTCR = 0.25*VINTMR
HSE = 0.0
NRTRI = 0
PEAI = 0.0
SPIF = 0.0
CBF = GWS*BFRL*(1.0 + BFNRL*BFNX)
SPDR = 0.0
OFUS = 0.0
OFUSIS = 0.0
OFR = 0.0
OFRIS = 0.0
PEIS = 0.0
RHFO = 0.0
URHF = 0.0
AMIF = 0.0
AMNET = 0.0
AMPET = 0.0
AMSNE = 0.0
AMFSIL = 0.0
SASFX = 0.0
SARAX = 0.0
SRX = CSRX
VWIN = 26.8888*AREA
WCFS = 24.0*VWIN
RHFCM = 0.025/WCFS
TFCFS = CBF*WCFS
SSRT = Sqrt(OFSS)
OFRF = 1020.0*SSRT/(OFMN*OFSL)
OFRFIS = 1020.0*SSRT/(OFMNIS*OFSL)**0.6)
EQDF = 0.00982*((OFMN*OFSL/SSRT)**0.6)
EQDFIS = 0.00982*((OFMNIS*OFSL/SSRT)**0.6)
  
```

```

SOFRF = OFRF
SOFRFI = OFRFIS
SDEPTH = 0.0
ASM = 0.0
IF(CONOPT(7) .EQ. 0) GO TO 116
WT4AM = 60.0
WT4PM = 60.0
SAX = 15.0
TANSM = 0.0
SPTW = 0.0
STMD = 0.7
SFMD = 0.7
ASMRG = 0.0
116 READ(5,2) TTITLE
2 FORMAT(20A4)
C BEGIN NEW YEAR
117 BYLZS = LZS
BYUZS = UZS
BYGWS = GWS
BYIFS = IFS
DO 118 KIA = 1,22
CRFMI(KIA) = 0.0
SESF(KIA) = 0.0
SERR(KIA) = 0.0
SERA(KIA) = 0.0
SQER(KIA) = 0.0
RGPM = RGPMB
DO 119 KIA = 1,21
T20DFH(KIA) = 0.0
T20PRH(KIA) = 0.0
DO 120 KIA = 1,12
EPCM(KIA) = 1.0
RDPT=0.0
PDAY=274
READ(5,2014) YR1,YR2
2014 FORMAT(2I3)
READ(5,2) YTITLE

```

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MAIN0118
MAIN0119
MAIN0120
MAIN0121
MAIN0122
MAIN0123
MAIN0124
MAIN0125
MAIN0126
MAIN0127
MAIN0128
MAIN0129
MAIN0130
MAIN0131
MAIN0132
MAIN0133
MAIN0134
MAIN0135
MAIN0136
MAIN0137
MAIN0138
MAIN0139
MAIN0140
MAIN0141
MAIN0142
MAIN0143
MAIN0144
MAIN0145
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MAIN0148
MAIN0149
MAIN0150
MAIN0152

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MAIN0154
 MAIN0155
 MAIN0156

 MAIN0157
 MAIN0158
 MAIN0159

 MAIN0160

 MAIN0161

MAIN0166
 MAIN0167
 MAIN0168
 MAIN0169
 MAIN0170
 MAIN0171
 MAIN0172
 MAIN0173
 MAIN0174
 MAIN0175
 MAIN0176
 MAIN0177
 MAIN0178
 MAIN0179
 MAIN0180

MAIN0182
 MAIN0183
 MAIN0184

DPY=365
 IF(MOD(YR2,4) .EQ. 0) DPY = 366
 IF(CONOPT(1) .EQ. 1) READ(5,2040) CDSDR,NDSDR
 2040 FORMAT(2I3)
 NDSDP = 0
 MEDWY(5) = 59
 IF(DPY .EQ. 366) MEDWY(5) = 366

C READ EVAPORATION DATA
 C
 C

IF(CONOPT(3) .NE. 1) GO TO 125
 121 READ(5,2015)(DPET(KRD),KRD=274,360,10)
 2015 FORMAT(4X,9F6.4)
 122 READ(5,2016)(DPET(KRD),KRD=1,273,10)
 2016 FORMAT(10F6.4)
 DO 124 IDAY2 = 1,9
 DO 123 IDAY1 = 274,360,10
 DAY = IDAY1 + IDAY2
 123 DPET(DAY) = DPET(IDAY1)
 DO 124 IDAY1 = 1,273,10
 DAY = IDAY1 + IDAY2
 IF(DAY .GT. 273) GO TO 124
 DPET(DAY) = DPET(IDAY1)
 124 CONTINUE
 DPET(366) = DPET(59)
 DPET(365) = DPET(363)
 DPET(364) = DPET(363)
 GO TO 127
 125 IF(CONOPT(3) .EQ. 2) GO TO 130
 DAY = 274
 126 READ(5,2017)DPET(DAY)
 2017 FORMAT(F6.4)
 IF(DAY .EQ. 273) GO TO 127
 CALL DAYNXT(DAY, DPY)
 GO TO 126

C READ MONTHLY PAN COEFFICIENTS.
 C

```

C 127 READ(5,2018)(EPCM(MONTH),MONTH=1,12)
2018 FORMAT(2X,12F5.2)
IF(EPAET.NE.0.0) GO TO 133
DO 129 DAY = 1,DPY
EPAET = EPAET + UPET(DAY)
IF(EPCM(6).NE.1.0) EPAET = 0.7*EPAET
GO TO 131
130 READ(5,2019)EPAET,MNRD
2019 FORMAT(2F5.2)
EMAET = EPAET*(365.0 + MNRD)/404.0
C CALL EVPDAY(DPET,EMAET)
C
C 131 AETX = 24.0*EPAET/365.0
AEX96 = 1.2*AETX
AEX90 = 0.3*AETX
SIAM = 1.2**SIAC
UZC = SUZC*AEX90 + BUZC*EXP(-2.7*LZS/LZC)
IF(UZC.LT.0.25) UZC = 0.25
SGRT = 0
DO 132 DAY = 1,366
DDIW(DAY) = 0.0
DRSF(DAY) = 0.0
DRGPM(DAY) = RGPMB
DRSGP(DAY) = 0.0
DC 132 HOUR = 1,24
132 DRHP(DAY,HOUR) = 0.0
133 IF(CONOPT(9).NE.1) GO TO 135
DAY = 274
DRSF(366) = 0.0

```

```

C READ DAILY RECORDED STREAMFLOW DATA.
C
C 134 READ(5,2020)DRSF(DAY)
2020 FORMAT(F7.0)
CALL DAYNXT(DAY,DPY)

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MAIN0187
MAIN0188
MAIN0189
MAIN0190
MAIN0191

MAIN0193

MAIN0194

MAIN0195
MAIN0196
MAIN0197
MAIN0198
MAIN0199
MAIN0200
MAIN0201
MAIN0202
MAIN0203
MAIN0204
MAIN0205
MAIN0206
MAIN0207
MAIN0208
MAIN0209
MAIN0210
MAIN0211

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MAIN0214
MAIN0215
MAIN0216
MAIN0217

MAIN0219
MAIN0220
MAIN0221
MAIN0222

MAIN0224
MAIN0225

MAIN0227

MAIN0230

MAIN0233

IF(DAY .NE. 274) GO TO 134
135 IF(CONOPT(11) .NE. 1) GO TO 137
DAY = 274

DDIW(366) = 0.0
136 RFAD(5,2021)DCIW(DAY)
2021 FORMAT(F5.0)

CALL DAYNXT(DAY, DPY)
IF(DAY .NE. 274) GO TO 136
137 IF(CONOPT(7) .EQ. 0) GO TO 139
DAY = 274

C
C READ DAILY MAX. AND MIN. TEMPERATURE.
C

138 READ(5,2022)DMXT(DAY),DMNT(DAY)
2022 FORMAT(2F5.0)
CALL DAYNXT(DAY, DPY)
IF(DAY .NE. 274) GO TO 138

C
C READ NUMBER OF STORAGE GAGE RAINFALL DAYS.
C

139 READ(5,2023)NSGRD
2023 FORMAT(I2)
IF(NSGRD .EQ. 0) GO TO 141
READ(5,2024)WSG,SGRT

2024 FORMAT(2F5.0)
IF(CONOPT(8) .EQ. 1) READ(5,2025) WSG2,SGRT2,SGMD
2025 FORMAT(3F5.0)

DO 140 KRD = 1,NSGRD
READ(5,2026)ISGRD
2026 FORMAT(I5)
140 READ(5,2030) DRSGP(ISGRD)
2030 FURMAT(F5.0)

C
C READ RECORDING RAIN GAGE HOURLY TOTALS
C

141 READ(5,2027)IWBG, YEAR, MONTH, DATE, CN
2027 FURMAT(I4, I2, I2, I2, I1)

MAIN0235
 MAIN0236
 MAIN0237
 MAIN0238
 MAIN0239

MAIN0242
 MAIN0243
 MAIN0244
 MAIN0245
 MAIN0246

MAIN0247

MAIN0248
 MAIN0249
 MAIN0250
 MAIN0251
 MAIN0252
 MAIN0253
 MAIN0254
 MAIN0255
 MAIN0256
 MAIN0257
 MAIN0258
 MAIN0259
 MAIN0260
 MAIN0261
 MAIN0262
 MAIN0263
 MAIN0264
 MAIN0265
 MAIN0266
 MAIN0267

C PUNCH NO NUMBER AFTER CN ON YEAR .EQ. 98 CARD

IF(YEAR .GE. 98) GO TO 144
 HRF = 12*(CN - 1) + 1
 HRL = 12*(CN - 1) + 12
 DAY = MEDCY(MONTH) + DATE
 142 READ(5,2028)(DRHP(DAY,HOUR), HOUR=HRF,HRL)
 2028 FORMAT(12F5.0)
 IF(DPY .NE. 366 .OR. MONTH .NE. 2 .OR. DATE .NE. 29) GO TO 141
 DO 143 HOUR = HRF, HRL
 DRHP(366,HOUR) = DRHP(60,HOUR)
 143 DRHP(60,HOUR) = 0.0
 GO TO 141

C CALCULATE PRECIPITATION WEIGHTING FACTORS

144 DAY = 274
 IF(NSGRD .EQ. 0) GO TO 151
 PDAY = 274
 RDPT = 0.0

145 EHS GD = SGRT
 IF(SGRT .EQ. 0) EHS GD = 24
 EHS GD F = EHS GD

146 CONTINUE
 DO 150 HOUR = 1,24
 RDPT = RDPT + DRHP(DAY,HOUR)
 IF(HOUR .NE. EHS GD) GO TO 150
 IF(RDPT .LE. 0.0) GO TO 147
 IF(SGRT .EQ. 0) PDAY = DAY
 DRGPM (PDAY) = (DRSGP(DAY)*WSG + RDPT*(1.0 - WSG))/RDPT
 IF(CONOPT(3) .NE. 0) DPET(PDAY) = 0.5*DPET(PDAY)
 IF(SGRT .NE. 0) PDAY = DAY
 RDPT = 0.0
 GO TO 150
 147 IF(DRSGP(DAY) .LE. 0.0) GO TO 149
 DO 148 KHOUR = 1,EHS GD

148 DRHP(DAY,KHCUR) = (WSG*DRSGP(DAY))/EHS GDF

149 IF(SGRT.NE.0) PDAY = DAY

150 CONTINUE

CALL DAYNXT(DAY,DPY)

IF(DAY.EQ.274) GO TO 151

IF(CONOPT(8).EQ.0) GO TO 146

IF(DAY.NE.SGMD) GO TO 146

WSG = WSG2

SGRT = SGRT2

GO TO 145

151 MCNTH = 1

MDAY = 273

AMRPM = 0.0

AMPREC = 0.0

AMBF = 0.0

AMSE = 0.0

AMSTF = 0.0

AMRTF = 0.0

WRITE(6,3) (TITLE(KTA), KTA = 1,20).

3 FFORMAT(1H,10X,20A4)

WRITE(6,4) (YTITLE(KTA), KTA = 1,20),YR1,YR2

4 FFORMAT(1H,20A4,2X,' WATER YEAR 19',12,'-',12)

WRITE(6,5)

5 FFORMAT(' OCTOBER ')

C

C BEGIN DAY LOOP

C

152 TDSF = 0.0

PET = EPCM(MONTH)*DPET(DAY)

PETU = PET

TFMAX = 0.0

C

C EVAPOTRANSPIRATION ADJUSTMENTS

C

IF(CONOPT(7).NE.1) GO TO 153

IF(DMXPT(DAY) - 4.0*ELDIF.LT.40.0) PET = 0.0

IF(SPTW.GT.SPTWCC) PET = FFOR*PET

MAIN0268
MAIN0269
MAIN0270
MAIN0271
MAIN0272
MAIN0273
MAIN0274
MAIN0275
MAIN0276
MAIN0277
MAIN0278
MAIN0279
MAIN0280
MAIN0281
MAIN0282
MAIN0283
MAIN0284
MAIN0285
MAIN0286
MAIN0287
MAIN0288
MAIN0289
MAIN0290

MAIN0292

MAIN0293

MAIN0294

MAIN0295

MAIN0296

MAIN0297

MAIN0298

MAIN0299

MAIN0300

MAIN0301

MAIN0302

MAIN0303

MAIN0304

MAIN0305

MAIN0306

MAIN0307

MAIN0308

MAIN0309

MAIN0310

MAIN0311

MAIN0312

MAIN0313

MAIN0314

MAIN0315

MAIN0316

MAIN0317

MAIN0318

MAIN0319

MAIN0320

MAIN0321

MAIN0322

MAIN0323

MAIN0324

MAIN0325

MAIN0326

MAIN0327

MAIN0328

MAIN0329

MAIN0330

MAIN0331

C CALCULATION OF SNOW EVAPORATION

IF(DMNT(DAY) .GT. 32.0 .OR. SPTW .LE. DPSE(DAY)) GO TO 153

SE = DPSE(DAY)

AMSNE = AMSNE + SE

SPTW = SPTW - SE

IF(SFMD .GT. 0.0) SDEPTH = SDEPTH - SE/SFMD

153 DO 202 HOUR = 1,24

IF((NSGRD .EQ. 0) .AND. (DRHP(DAY,HOUR) .NE. 0.0) .AND. (PET .EQ. 0.5*PET

1 PETU) .AND. (CONOPT(3) .EQ. 1)) PET = 0.5*PET

154 IF(HOUR .EQ. SGRT + 1) RGPM = DRGPM(DAY)

IF(HOUR .EQ. 9) HSE = (FWTR*PET)/12.0

IF(HOUR .EQ. 21) HSE = 0.0

PRH = RGPM*DRFP(DAY,HOUR)

AMPREC = AMPREC + PRH

C ENTER SNOWMELT SUBROUTINE

C

IF(CONOPT(7) .EQ. 1) CALL SNCMEL(BDDFSM,SPTWCC,SPM,ELDIF,DAY,

1 SPBFLW,XDNFS,FFOR,FFSI,MRNSM,DSMGH,SDEPTH,STMD,PXCSA,HOUR,

2 SAX,SOFRF,OFRFIS,SOFRFI,AMFSIL,PRH,SPTW,TANSM,SPLW,SFMD,OFRF,

3 WT4AM,WT4PM,ASM,ASMRG,SASFX,SARAX,DMXT,DMNT,RICY,FIRR)

155 AMRPM = AMRPM + PRH

156 TOFR = 0.0

ARHF = 0.0

C 15 MINUTE ACCOUNTING AND ROUTING LOOP

C

DO 187 PRD = 1,4

PEBI = 0.0

PPI = 0.0

OFR = 0.0

OFRFIS = 0.0

WI = 0.0

WEIFS = 0.0

PMEUFS = 0.0

MAIN0332
 MAIN0333
 MAIN0334
 MAIN0335
 MAIN0336
 MAIN0337
 MAIN0338
 MAIN0339
 MAIN0340
 MAIN0341
 MAIN0342
 MAIN0343
 MAIN0344

 MAIN0345

 MAIN0346
 MAIN0347
 MAIN0348
 MAIN0349
 MAIN0350
 MAIN0351
 MAIN0352
 MAIN0353
 MAIN0354
 MAIN0355
 MAIN0356
 MAIN0357
 MAIN0358
 MAIN0359
 MAIN0360
 MAIN0361
 MAIN0362
 MAIN0363
 MAIN0364
 MAIN0365

```

PME LZS = 0.0
PME IFS = 0.0
PME OFS = 0.0
PEP = 0.25*PRH
IF(CONOPT(2) .EQ. 1) CALL PREPRD(RGPM,DRHP, DAY,HOUR,DPY,PRD,PEP,
1 PRH)
IF(PEP .GT. 0.0) GO TO 157
IF(OFUS .GT. 0.0) GO TO 159
IF(IFS .GT. 0.0) GO TO 170
IF(NRTRI .GT. 0) GO TO 172
TPHF = 0.0
IF(RHFO .GT. 0.0) GO TO 181
GO TO 184
  
```

C RAINFALL UPPER ZCNE INTERACTION

```

157 IF(PEP .GE. VINTCR) GO TO 158
    UZS = UZS + PEP*TPLR
    VINTCR = VINTCR - PEP
    PPI = 0.0
    PEBI = 0.0
    PME UZS = PEP
    IF(OFUS .GT. 0.0) GO TO 159
    GO TO 170
  
```

```

158 PPI = PEP - VINTCR
    UZS = UZS + VINTCR*TPLR
    VINTCR = 0.0
    LZSR = LZS/LZC
    UZC = SUZC*AEX90 + BUZC*EXP(-2.7*LZSR)
    IF(UZC .LT. 0.25) UZC = 0.25
    UZRX = 2.0*ABS(UZS/UZC - 1.0) + 1.0
    FMR = (1.0/(1.0 + UZRX))**UZRX
    IF(UZS .GT. UZC) FMR = 1.0 - FMR
    PEBI = PPI*FMR
    PME UZS = PEP - PEBI
    UZS = UZS + PPI - PEBI
  
```

C

C LOWER ZONE AND GROUNDWATER INFILTRATION

MAIN0366
 MAIN0367
 MAIN0368
 MAIN0369
 MAIN0370
 MAIN0371
 MAIN0372

```

159 LZSR = LZS/LZC
    EID = 4.0*LZSR
    IF(LZSR .LE. 1.0) GO TO 160
    EID = 4.0 + 2.0*(LZSR - 1.0)
    IF(LZSR .LE. 2.0) GO TO 160
    EID = 6.0
    
```

C WATER ENTERING AS INFILTRATION, INTERFLOW, AND DIRECT RUNOFF.

MAIN0373
 MAIN0374
 MAIN0375
 MAIN0376
 MAIN0377
 MAIN0378
 MAIN0379
 MAIN0380
 MAIN0381
 MAIN0382
 MAIN0383
 MAIN0384
 MAIN0385
 MAIN0386

```

160 PEBI = PEBI + OFUS
    CMIR = 0.25*SIAM*BMIR/(2.0**EID)
    CIVM = BIVF*2.0**LZSR
    IF(CIVM .LT. 1.0) CIVM = 1.0
    PEAI = PEBI*PEBI/(2.0*CMIR*CIVM)
    WI = PEBI*PEBI/(2.0*CMIR)
    IF(PEBI .GE. CMIR) WI = PEBI - 0.5*CMIR
    IF(PEBI .GE. CMIR*CIVM) PEAI = PEBI - 0.5*CMIR*CIVM
    WEIFS = WI - PEAI
    IF(PEBI .LE. OFUS) GO TO 161
    PМЕLZS = (PEBI - WI)*((PEBI - OFUS)/PEBI)
    PМЕIFS = WEIFS*((PEBI - OFUS)/PEBI)
    PМЕOFS = PEAI*((PEBI - OFUS)/PEBI)
    
```

161 CONTINUE

C EQUILIBRIUM SURFACE DETENTION STORAGE.

MAIN0387
 MAIN0388
 MAIN0389
 MAIN0390
 MAIN0391
 MAIN0392

```

    IF((PEAI - OFUS) .GT. 0.0) GO TO 162
    EQD = (OFUS + PEAI)/2.0
    GO TO 163
162 EQD = EQDF*((PEAI - OFUS)**0.6)
163 IF((OFUS + PEAI) .GT. (2.0*EQD)) EQD = 0.5*(OFUS + PEAI)
    IF((OFUS + PEAI) .LE. 0.001) GO TO 164
    
```

C OVERLAND FLOW FROM PERVIOUS SURFACES.

MAIN0393
MAIN0394
MAIN0395

```

OFR = 0.25*OFRF*((OFUS + PEAI)*0.5)**1.67)*((1.0 + 0.6*((OFUS +
1 PEAI)/(2.0*EQD))**3.0)**1.67)
IF(OFR .GT. (0.75*PEAI)) OFR = 0.75*PEAI

```

C OVERLAND FLOW FROM IMPERVIOUS SURFACES.

MAIN0396
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MAIN0398
MAIN0399
MAIN0400
MAIN0401
MAIN0402
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MAIN0404
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MAIN0407
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MAIN0409
MAIN0410
MAIN0411
MAIN0412
MAIN0413
MAIN0414

```

164 IF(FIMP .EQ. 0.0) GO TO 168
165 PEIS = PPI + OFUSIS
IF((PEIS - OFUSIS) .GT. 0.0) GO TO 166
EQDIS = (OFUSIS + PEIS)/2.0
GO TO 167
166 EQDIS = EQDIS*((PEIS - OFUSIS)**0.6)
167 IF((OFUSIS + PEIS) .GT. (2.0*EQDIS)) EQDIS = 0.5*((OFUSIS + PEIS)
IF((OFUSIS + PEIS) .LE. 0.01) GO TO 168
OFRIS = 0.25*CFRFRIS*((OFUSIS + PEIS)*0.5)**1.67)*((1.0 + 0.6*((
1 OFUSIS + PEIS)/(2.0*EQDIS))**3.0)**1.67)
IF(OFRIS .GT. PEIS) OFRIS = PEIS
168 TOFR = TOFR + FPER*OFR + FIMP*OFRIS + PPI*FWTR
OFUSIS = PEIS - OFRIS
OFUS = PEAI - OFR
IF(OFUS .GE. 0.001) GO TO 169
LZS = LZS + OFUS
OFUS = 0.0
OFRIS = OFRIS + OFUSIS
OFUSIS = 0.0

```

C QUANTITIES RETAINED IN VARIOUS SOIL LOCATIONS.

MAIN0415
MAIN0416
MAIN0417
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MAIN0419
MAIN0420
MAIN0421
MAIN0422
MAIN0423

```

169 LZR X = 1.5*ABS(LZS/LZC - 1.0) + 1.0
FMR = (1.0/(1.0 + LZR X))*LZR X
IF(LZS .LT. LZC) FMR = 1.0 - FMR*(LZS/LZC)
PLZS = FMR*((PEBI - WI)
PGW = (1.0 - FMR)*(PEBI - WI)*(1.0 - SUBWF)*FPER
GWS = GWS + PGW
BFNX = BFNX + PGW
LZS = LZS + PLZS
IFS = IFS + WEIFS*FPER

```

```

170 SPIF = IFRL*IFS
    AMIF = AMIF + SPIF
    IFS = IFS - SPIF
    IF(IFS .GE. 0.0001) GO TO 171
    LZS = LZS + IFS
    IFS = 0.0
171 UHFA(1) = FPER*OFR + PPI*FWTR + FIMP*OFRIS + SPIF
    SPDR = UHFA(1)
C
C ROUTING
C
172 IF(CONOPT(12) .NE. 1) GO TO 173
    URHF = URHF + 0.25*UHFA(1)
    IF(PRD .NE. 4) GO TO 181
    UHFA(1) = URHF
173 TRHF = 0.0
    KTRI = NCSTRI
    IF(CONOPT(13) .EQ. 1) KTRI = NCSTRI
174 URHF = UHFA(KTRI)
    IF(URHF .LE. 0.0) GO TO 176
175 TRHF = TRHF + URHF*CTRI(KTRI)
    IF(CONOPT(13) .EQ. 1 .AND. LSHFT .AND. KTRI .GE. 2) TRHF = TRHF +
        1 URHF*SATRI(KTRI - 1)
    UHFA(KTRI + 1) = URHF
    GO TO 177
176 UHFA(KTRI + 1) = 0.0
177 KTRI = KTRI - 1
    IF(KTRI .GE. 1) GO TO 174
178 IF(URHF .LE. 0.0) GO TO 179
    NRTRI = NCSTRI
    IF(CONOPT(13) .EQ. 1) NRTRI = MXTRI
179 NRTRI = NRTRI - 1
    UHFA(1) = 0.0
    IF(CONOPT(13) .NE. 1) GO TO 180
    NNSTRI = NCSTRI + 1
    UHFA(NNSTRI) = 0.0
180 URHF = 0.0

```

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 MAIN0458

```

181 IF(SRX .LE. CSRX) SRX = CSRX
    RHFI = TRHF - SRX*(TRHF - RHFO)
    RHFO = RHFI
    IF(RHFO .LT. RHFC) RHFO = 0.0
    TFCFS = (4.0*RHFI + CBF - HSE)*WCFS
    IF(CONOPT(13) .NE. 1) GO TO 182
    IF(CONOPT(12) .EQ. 1 .AND. PRD .NE. 4) GO TO 182
    CALL RTVARY (CTRI,SATRI,BTRI,CHCAP,NBTRI,NCSTRI,EXQPV,LSHFT,
1 TFCFS)
    DATE = MOD(DAY,MDAY)
    IF(LSHFT) WRITE(6,6) DATE,HOUR,PRD,NCSTRI
6 FORMAT(2X,I2,2X,I2,2X,I2,2X, ' HISTOGRAM CHANGES TO',I2,I2,I2,1X,
1 ' ELEMENTS')
182 CONTINUE
    IF(TFCFS .LE. 0.5*CHCAP) SRX = CSRX
    IF((TFCFS .GT. 0.5*CHCAP) .AND. (TFCFS .LT. 2.0*CHCAP)) SRX = CSRX
    I +(FSRX - CSRX)*((TFCFS - 0.5*CHCAP)/(1.5*CHCAP))*3
    IF(TFCFS .GT. 2.0*CHCAP) SRX = FSRX
    IF(TFCFS .LE. TFMAX) GO TO 183
    PRDF = PRD
    TDFP24 = HOUR
    IF(PRD .LE. 3) TDFP24 = (TDFP24 - 1.0) + 0.15*PRDF
    TFMAX = TFCFS
183 ARHF = ARHF + RHFI

C STORM OUTPUT REQUESTED BY CONOPT(1)
C
C
184 IF(CONOPT(1) .NE. 1) GO TO 186
    IF(DAY .NE. CSDR) GO TO 186
    IF(HOUR .EQ. 1 .AND. PRD .EQ. 1) WRITE(6,7)
7 FORMAT(1H, 21X, 'RAINFALL DEPOSITION',I2X, 'MOISTURE STORAGE',
1 14X, 'STREAMFLOW ORIGIN',6X, 'STREAM OUTFLOW',2X, ' DY HR PD RA
2IN EUZS ELZS EIFS EOFS UZS LZS IFS
3POF SPIF SPBF SPTF INCHES CFS ')
    DATE = MOD(DAY,MDAY)
    OFS = OFUS*FPER + OFUSIS*FIMP
    SPOF = OFR*FPER + OFRIS*FIMP + PPI*FWTR

```

```

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```

C READ IN OVERLAND FLOW PARAMETERS.

C READ(5,2011) CFSS,OFSL,OFMN,OFMNIS,IFRC
C 2011 FORMAT(5F10.3)

C READ IN CHANNEL ROUTING AND GROUNDWATER PARAMETERS.

C READ(5,2012) CSRX,FSRX,CHCAP,EXQPV,BFNLR,BFRC
C 2012 FORMAT(6F10.5)
C BFHRC=BFRC*(1.0/24.0)
C BFRL = -ALOG(BFHRC)

C BFNRL = 0.0
C IF(BFNLR.LT. 0.00001 .OR. BFNLR .GT. 0.9999) GO TO 111
C BFNHR = BFNLR*(1.0/24.0)
C BFNRL = -ALOG(BFNHR)
C 111 IFPRC = IFRC*(1.0/96.0)
C IFRL = -ALOG(IFPRC)

C STARTING MOISTURE STORAGE VALUES AS OF OCTOBER 1.

C READ(5,2013) GWS,UZS,LZS,BFNX,IFS

C 2013 FORMAT(5F5.0)

LSHFT = .FALSE.

IF(CONOPT(13) .NE. 1) GO TO 113

NBTRI = NCTRI

FNTRI = NCTRI

MXTRI = (10.0**EXQPV)*FNTRI + 0.5

IF(MXTRI .GE. 98) WRITE(6,1)

1 FORMAT(, WARNING: EXQPV ARRAY OVER RUN ')

NCSTRI = 99

DO 112 KIA = 1, NBTRI

BTRI(KIA) = CTRI(KIA)

TFCFS = 1.0

CALL RTVARY (CTRI,SATRI,BTRI,CHCAP,NBTRI,MXTRI,NCSTRI,EXQPV,LSHFT,
1 TFCFS)

1 TFCFS)

113 EPAET=0.0

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```

SPBF = 0.25*(CBF-HSE)
SPTF = SPDR + SPBF
SPDR = 0.0
IF(RHFO .LE. 0.0) TFCFS = (CBF - HSE)*WCFS
RSPTF = 0.25*TFCFS/WCFS
WRITE(6,8) DATE,HOUR,PRD,PEP,PMELZS,PMELZS,PMEIFS,PMEOFS,UZS,LZS
1,IFS,OFS,SPCF,SPIF,SPBF,SPTF,RSPTF,TFCFS
8 FFORMAT(2X,I2,1X,I2,1X,I1,5(1X,F6.4),2X,4(F7.4),2X,5(1X,F6.4),1X,
1 F7.1)
IF(HOUR .EQ. 24 .AND. PRD .EQ. 4) GO TO 185
GO TO 186
185 NDSDP = NDSDP + 1
IF(NDSDR .EQ. NDSDP) GO TO 186
CALL DAYNXT(CDSOR,DPY)
186 CONTINUE
IF(VINTCR .LT. 0.25*VINTMR) VINTCR = VINTCR + DPET(DAY)/96.0
187 CONTINUE
C
C END OF 15 MINUTE LOOP
C
IF(CONOPT(5) .NE. 1) GO TO 197
C
C HOURLY OVERLAND FLOW AND RAINFALL SORTING
C
IF(TOFR .LE. 0.0) GO TO 193
KT20 = 20
188 IF(KT20 .LT. 1) GO TO 192
IF(TOFR .GT. T200FH(KT20)) GO TO 189
GO TO 190
189 T200FH(KT20+1) = T200FH(KT20)
GO TO 191
190 T200FH(KT20+1) = TOFR
GO TO 193
191 KT20 = KT20 - 1
GO TO 188
192 T200FH(1) = TOFR
193 IF(PRH .LE. 0.0) GO TO 197

```



```

C      4 PM ADJUSTMENTS OF VARIOUS VALUES
C
C      198 IF(HOUR .NE. 16) GO TO 202
C      AEX90 = 0.9*(AEX90 + PET)
C      AEX96 = 0.96*(AEX96 + PET)
C
C      INFILTRATION CORRECTION
C
C      SIAM = (AEX96/AETX)**SIAC
C      IF(SIAM .LT. 0.33) SIAM = 0.33
C      BFNX = 0.97*BFNX
C      IF(PET .EQ. 0.0) GO TO 202
C
C      EVAP-TRANS LOSS FROM GROUNDWATER
C
C      GWET = GWS*GWETF*PET*FFPER
C      GWS = GWS - GWET
C      BFNX = BFNX - GWET
C      IF(BFNX .LT. 0.0) BFNX = 0.0
C      AMPET = AMPET + PET
C      IF(PET .GE. UZS) GO TO 199
C      UZS = UZS - PET
C      AMNET = AMNET + PET
C      GO TO 202
C      199 PET = PET - UZS
C      AMNET = AMNET + UZS
C      UZS = 0.0
C      LZSR = LZS/LZC
C      IF(PET .GE. ETLF*LZSR) GO TO 200
C      SET = PET*(1.0 - PET/(2.0*ETLF*LZSR))
C      GO TO 201
C      200 SET = 0.5*ETLF*LZSR
C      201 LZS = LZS - SET
C      AMNET = AMNET + SET
C      202 CONTINUE
C

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```

C END OF HOUR LOOP
C
DSSF(DAY) = TDSF/24.0
IF(CONOPT(11) .EQ. 1) DSSF(DAY) = DSSF(DAY) + DDIW(DAY)
203 AMRTF = AMRTF + DRSF(DAY)
AMSTF = AMSTF + DSSF(DAY)
IF(CONOPT(6) .EQ. 1) EDLZS(DAY) = LZS
C
C STORE ERRORS AND FLOW DURATION
C
IF(CONOPT(4) .NE. 1) GO TO 204
ERR = DSSF(DAY) - DRSF(DAY)
IF(DRSF(DAY) .LT. 1.0) KRPMI = 1.0
IF(DRSF(DAY) .GT. 1.0) KRPMI = 2.0*ALOG(DRSF(DAY)) + 2.0
CRPMI(KRPMI) = CRPMI(KRPMI) + 1.0
SERR(KRPMI) = SERR(KRPMI) + ERR
SERA(KRPMI) = SERA(KRPMI) + ABS(ERR)
SQER(KRPMI) = SQER(KRPMI) + ERR*ERR
SESF(KRPMI) = 0.0
IF(CRFMI(KRPMI) .GT. 1.0) SESF(KRPMI) = SQRT(ABS((SQER(KRPMI) -
1 SERR(KRPMI))*2/CRFMI(KRPMI)))/(CRFMI(KRPMI) - 1.0))
204 IF(DAY .EQ. 366) MDAY = 337
DATE = MOD(DAY,MDAY)
IF(TFMAX .LE. RMPF) GO TO 206
WRITE(6,9) DATE, (THSF(HOUR), HOUR=1,12)
9 FOPMAT(1H,1X,1X,1X,14,2X,'AM',1X,6F8.1,3X,6F8.1)
WRITE(6,10) (THSF(HOUR), HOUR=13,24), DSSF(DAY)
10 FOPMAT(1H1,6X,'PM',1X,6F8.1,3X,7F8.1)
IF(TDFP24 .LT. 12.0) GO TO 205
TDFP12 = TDFP24 - 12.0
WRITE(6,11) TFMAX, TDFP12
11 FOPMAT(1H/,10X,'MAXIMUM=',F8.1,2X,'C.F.S.',5X,'TIME',3X,F5.2,2X,
1 ' P.M. ')
GO TO 206
205 WRITE(6,12) TFMAX, TDFP24
12 FOPMAT(1H,10X,'MAXIMUM=',F8.1,2X,'C.F.S.',5X,'TIME',3X,F5.2,2X,
1 ' A.M. ')

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206 IF(CONOPT(7) .EQ. 1 .AND. SDEPTH .GT. 0.0) WRITE(6,13)DATE,
1 SDEPTH,STMD,SAX,TANSM,SPLW
13 FORMAT(3X,I4,2X,'SDEPTH=',F8.2,2X,'STMD=',F6.2,2X,'SAX=',F6.2,
1 2X,'TANSM=',F6.2,2X,'SPLW=',F6.2)
  
```

C MONTHLY SUMMARY STORAGE

```

C
C IF(DAY .NE. MEDWY(MONTH)) GO TO 220
C TMSTF(MONTH) = AMSTF
C AMSTF = 0.0
C TMRTF(MONTH) = AMRTF
C AMRTF = 0.0
C EMBFNX(MONTH) = BFNX
C TMPREC(MONTH) = AMPREC
C AMPREC = 0.0
C TMRPN(MONTH) = AMRPM
C AMRPM = 0.0
C TMBF(MONTH) = AMBF
C AMBF = 0.0
C TMIF(MONTH) = AMIF
C AMIF = 0.0
C TMSE(MONTH) = AMSE
C AMSE = 0.0
C TMPET(MONTH) = AMPET
C AMPET = 0.0
C TMNET(MONTH) = AMNET
C AMNET = 0.0
C TMSNE(MONTH) = AMSNE
C AMSNE = 0.0
C TMSIL(MONTH) = AMFSIL
C AMFSIL = 0.0
C EMGWS(MONTH) = GWS
C UZC = SUZC*AE90 + BUZC*EXP(-2.7*LZS/LZC)
C IF(UZC .LT. 0.25) UZC = 0.25
C EMUZC(MONTH) = UZC
C EMUZS(MONTH) = UZS
C EMSIAM(MONTH) = SIAM
  
```

MAIN0659
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```

EMLZS(MONTH) = LZS
EMIFS(MONTH) = IFS
IF(MONTH.EQ.5) MEDWY(5) = 59
MDAY = MEDWY(MONTH)
207 IF(MONTH.NE.0) GO TO (208,209,210,211,212,213,214,215,216,217,
1 218,219),MONTH
208 WRITE(6,14)
14 FORMAT(1H,'NOVEMBER')
GO TO 219
209 WRITE(6,15)
15 FORMAT(1H,'DECEMBER')
GO TO 219
210 WRITE(6,16)
16 FORMAT(1H,'JANUARY')
GO TO 219
211 WRITE(6,17)
17 FORMAT(1H,'FEBRUARY')
GO TO 219
212 WRITE(6,18)
18 FORMAT(1H,'MARCH')
GO TO 219
213 WRITE(6,19)
19 FORMAT(1H,'APRIL')
GO TO 219
214 WRITE(6,20)
20 FORMAT(1H,'MAY')
GO TO 219
215 WRITE(6,21)
21 FORMAT(1H,'JUNE')
GO TO 219
216 WRITE(6,22)
22 FORMAT(1H,'JULY')
GO TO 219
217 WRITE(6,23)
23 FORMAT(1H,'AUGUST')
GO TO 219
218 WRITE(6,24)
  
```

MAIN0696
 MAIN0697
 MAIN0698
 MAIN0699

 MAIN0700

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 MAIN0702
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 MAIN0704
 MAIN0705
 MAIN0706

 MAIN0707

 MAIN0708
 MAIN0709
 MAIN0710
 MAIN0711
 MAIN0712
 MAIN0713
 MAIN0714
 MAIN0715
 MAIN0716
 MAIN0717
 MAIN0718
 MAIN0719
 MAIN0720
 MAIN0721
 MAIN0722
 MAIN0723
 MAIN0724
 MAIN0725
 MAIN0726
 MAIN0727
 MAIN0728

```

24 FORMAT(1H, 'SEPTEMBER')
219 MONTH = MONTH + 1
220 CALL DAYNXT(DAY,DPY)
    IF(DAY .NE. 274) GO TO 152
C
C END OF DAY LOOP
C
221 CONTINUE
222 WRITE(6,25) (TITLE(KTA), KTA=1,20,1)
25 FCRMAT(1H1,10X,20A4)
    WRITE(6,26) (YTITLE(KTA),KTA=1,15,1),YR1,YR2
26 FORMAT(1H,15A4,3X,'WATER YEAR 19',I2,1H-',I2,7X,
1,' KENTUCKY WATERSHED MODEL ',)
  
```

C ANNUAL SUMMARY

```

SATFV = 0.0
RATFV = 0.0
APREC = 0.0
ABFV = 0.0
ARPM = 0.0
ASEV = 0.0
ANET = 0.0
APET = 0.0
AIFV = 0.0
ASE = 0.0
AFSIL = 0.0
DO 223 MONTH = 1,12
SATFV = SATFV + TMSIF(MONTH)
RATFV = RATFV + TMRIF(MONTH)
APREC = APREC + TMPREC(MONTH)
ABFV = ABFV + TMBF(MONTH)
ARPM = ARPM + TMRPM(MONTH)
ASEV = ASEV + TMSE(MONTH)
ANET = ANET + TMNET(MONTH)
APET = APET + TMPET(MONTH)
AIFV = AIFV + TMIF(MONTH)
  
```

MAIN0729
 MAIN0730
 MAIN0731
 MAIN0732
 MAIN0733
 MAIN0734
 MAIN0735
 MAIN0736
 MAIN0737
 MAIN0738
 MAIN0739
 MAIN0740
 MAIN0741
 MAIN0742
 MAIN0743
 MAIN0744
 MAIN0745
 MAIN0746
 MAIN0747
 MAIN0748
 MAIN0749
 MAIN0750
 MAIN0751
 MAIN0752
 MAIN0753
 MAIN0754
 MAIN0755
 MAIN0756
 MAIN0757
 MAIN0758
 MAIN0759
 MAIN0760
 MAIN0761
 MAIN0762
 MAIN0763
 MAIN0764
 MAIN0765

```

    ASE = ASE + TMSNE(MONTH)
223 AFSIL = AFSIL + TMSIL(MONTH)
    IF(CONOPT(14) .NE. 1) GO TO 224
    WRITE(6,27)
27  FORMAT(1H, '//44X, 'RECORDED
    CALL DAYOUT(DRSF, MEDWY, DPY)
    WRITE(6,28)
224  FORMAT(1H, '//44X, 'SYNTHESIZED
    CALL DAYOUT (DSSF, MEDWY, DPY)
    WRITE(6,29) (TMSTF(KWD), KWD=1,12), SATFV
29  FORMAT(1H, 'IX, 'SYNTHETIC', 3X, 12F8.1, 2X, F10.1, 2X, 'SFD')
    DO 225 MONTH = 1, 12
225  TMSTFI(MONTH) = (TMSTF(MONTH))/VWIN
    SATFVI = SATFV/VWIN
    WRITE(6,30) (TMSTFI(KWD), KWD=1,12), SATFVI
30  FORMAT(1X, 'TOTAL', 8X, 12F8.3, 4X, F7.3, 2X, 'INCHES')
    DO 226 MONTH = 1, 12
    TMOF(MONTH) = TMSIFI(MONTH) - TMIF(MONTH) - TMBF(MONTH) +
1  TMSE(MONTH)
226  IF(TMOF(MONTH) .LT. 0.0) TMOF(MONTH) = 0.0'
    AOFV = SATFVI - AIFV - ABFV + ASEV
    IF(AOFV .LT. 0.0) AOFV = 0.0
    WRITE(6,31) (TMOF(KWD), KWD=1,12), AOFV
31  FORMAT(1X, 'OVERLAND', 5X, 12F8.3, 4X, F7.3, 2X, 'INCHES')
    WRITE(6,32) (TMIF(KWD), KWD=1,12), AIFV
32  FORMAT(1X, 'INTERFLOW', 4X, 12F8.3, 4X, F7.3, 2X, 'INCHES')
    WRITE(6,33) (TMBF(KWD), KWD=1,12), ABFV
33  FORMAT(1X, 'BASE', 9X, 12F8.3, 4X, F7.3, 2X, 'INCHES')
    WRITE(6,34) (TMSE(KWD), KWD=1,12), ASEV
34  FORMAT(1X, 'STRM EVAP', 4X, 12F8.3, 4X, F7.3, 2X, 'INCHES')
    IF(CONOPT(9) .EQ. 0) GO TO 227
    WRITE(6,35) (TMRTF(KWD), KWD=1,12), RATFV
35  FORMAT(1X, 'RECORDED', 4X, 12F8.1, 2X, F10.1, 2X, 'SFD')
    RATFVI = RATFV/VWIN
    WRITE(6,36) RATFVI
36  FORMAT(112X, F9.2, 2X, 'INCHES')
227  WRITE(6,37) (TMPREC(KWD), KWD=1,12), APREC
  
```

MAIN0766
 MAIN0767
 MAIN0768
 MAIN0769
 MAIN0770
 MAIN0771
 MAIN0772
 MAIN0773
 MAIN0774
 MAIN0775
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 MAIN0777
 MAIN0778
 MAIN0779
 MAIN0780
 MAIN0781
 MAIN0782
 MAIN0783
 MAIN0784
 MAIN0785
 MAIN0786
 MAIN0787
 MAIN0788
 MAIN0789
 MAIN0790
 MAIN0791
 MAIN0792
 MAIN0793
 MAIN0794
 MAIN0795
 MAIN0796
 MAIN0797
 MAIN0798
 MAIN0799
 MAIN0800
 MAIN0801
 MAIN0802

```

37 FORMAT(IX,'PRECIP',7X,12F8.2,3X,F8.2,2X,'INCHES')
   IF(CONOPT(7).EQ.1) WRITE(6,38) (TMRPM(KWD), KWD=1,12),ARPM
38 FORMAT(IX,'RAIN+MELT',4X,12F8.2,3X,F8.2,2X,'INCHES')
   IF(CONOPT(7).EQ.1) WRITE(6,39) (TMSNE(KWD), KWD=1,12),ASE
39 FORMAT(IX,'SURSNOWEVAP',3X,12F8.3,3X,F7.3,2X,'INCHES')
   IF(CONOPT(7).EQ.1) WRITE(6,40) (TMFSIL(KWD), KWD=1,12),AFSIL
40 FORMAT(IX,'INTSNOWLOSS',3X,12F8.3,3X,F7.3,2X,'INCHES')
   WRITE(6,41) (TMNET(KWD), KWD=1,12),ANET
41 FORMAT(IX,'EVP/TRAN-NET',2X,12F8.3,3X,F7.3,2X,'INCHES')
   WRITE(6,42) (TMPET(KWD), KWD=1,12),APET
42 FORMAT(3X,10H-POTENTIAL,2X,12F8.3,3X,F7.3,2X,'INCHES')
   WRITE(6,43) (EMUZS(KWD), KWD=1,12)
43 FORMAT(IX,'STORAGES-UZS',2X,12F8.3,12X,'INCHES')
   WRITE(6,44) (EMLZS(KWD), KWD=1,12)
44 FORMAT(10X,'LZS',2X,12F8.3,12X,'INCHES')
   WRITE(6,45) (EMIFS(KWD), KWD=1,12)
45 FORMAT(10X,'IFS',2X,12F8.3,12X,'INCHES')
   WRITE(6,46) (EMGWS(KWD), KWD=1,12)
46 FORMAT(10X,'GWS',2X,12F8.3,12X,'INCHES')
   WRITE(6,47) (EMUZC(KWD), KWD=1,12)
47 FORMAT(IX,'INDICES-UZC',2X,12F8.3)
   WRITE(6,48) (EMBNX(KWD), KWD=1,12)
48 FORMAT(9X,'BFNX',2X,12F8.3)
   WRITE(6,49) (EMSIAM(KWD), KWD=1,12)
49 FORMAT(9X,'SIAM',2X,12F8.3)
   IF(CONOPT(7).NE.1) SPM = 1.0
   AMBER = (LZS - BYLZS + IFS - BYIFS)*FPER + (UZS - BYUZS + GWS -
1 BYGWS)*(1.0 - FWTR) + SATFV/VWIN + ANET*FPER + ASEV - APREC
2 + ASE + AFSIL - ((SPM - 1.0)/SPM)*ASM
   WRITE(6,50) AMBER
50 FORMAT(1H,'BALANCE',5X,F10.4,2X,'INCHES')
   IF(CONOPT(7).NE.1) GO TO 228
   WRITE(6,51) ASM, ASMRG
51 FORMAT(1H,'CHECK ON SNOW',5X,F10.4,5X,F10.4)
   ASM = 0.0
   ASMRG = 0.0
228 CONTINUE
  
```

```

IF(CONOPT(4) .NE. 1) GO TO 232
WRITE(6,52)
52 FORMAT(1H1,10X, 'DAILY FLOW DURATION AND ERROR TABLE')
WRITE(6,53)
53 FORMAT(1H/,10X, 'FLOW INTERVAL',5X,'CASES',3X,'AV.ERROR',3X,
1 'AVR. ABS. ERROR',3X, 'STANDARD ERROR')
SSESF = 0.0
SSERA = 0.0
SSERR = 0.0
ACRFMI = 0.0
DO 230 KRFMI = 1,22
IF(KRFMI .EQ. 1) ETIBF = 0.0
IF(KRFMI .EQ. 2) ETIBF = 1.0
FKRFMI = KRFMI
IF(KRFMI .GT. 2) ETIBF = EXP((FKRFMI/2.0) - 1.0)
CCRFMI = CCRFMI(KRFMI)
IF(CCRFMI .EQ. 0.0) WRITE(6,54) ETIBF, CCRFMI
54 FORMAT(1H,1X,13X,F8.1,1H-,F9.1,F12.1,5X,F8.2,5X,F8.2)
IF(CCRFMI .EQ. 0.0) GO TO 229
SERAV = SERA(KRFMI)/CCRFMI
SERRV = SEPR(KRFMI)/CCRFMI
IF(CCRFMI .EQ. 1) WRITE(6,54) ETIBF,CCRFMI,SERRV,SERAV
IF(CCRFMI .NE. 1) WRITE(6,54) ETIBF,CCRFMI,SERRV,SERAV,
1SESF(KRFMI)
229 ACRFMI = ACRFMI + CRFMI(KRFMI)
IF(ACRFMI .EQ. 0.0) GO TO 230
SSERR = SSERR + SERR(KRFMI)
SSERRV = SSERR/ACRFMI
SSERA = SSERA + SERA(KRFMI)
SSERAV = SSERA/ACRFMI
230 SSESF = SSESF + SESF(KRFMI)
WRITE(6,55) ACRFMI,SSERRV,SSERAV,SSESF
55 FORMAT(1H,22X,F9.1,F12.1,5X,F8.2,5X,F8.2)
FDPY = DPY
SADF = SATFV/FDPY
RADF = RATFV/FDPY
RA1 = 0.0

```

```

MAIN0803
MAIN0804
MAIN0805
MAIN0806
MAIN0807
MAIN0808
MAIN0809
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MAIN0838
MAIN0839

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MAIN0840
 MAIN0841
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MAIN0853

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 MAIN0857
 MAIN0858
 MAIN0859
 MAIN0860
 MAIN0861
 MAIN0862
 MAIN0863
 MAIN0864
 MAIN0865
 MAIN0866
 MAIN0867
 MAIN0868
 MAIN0869
 IDAH0009
 IDAH0010
 MAIN0871

 DYNX0001

```

RA2 = 0.0
RA3 = 0.0
DC 231 DAY = 1,DPY
DRAF = DRSF(DAY) - RADF
DSAF = DSSF(DAY) - SADF
RA1 = RA1 + DRAF*DRAF
RA2 = RA2 + DSAF*DSAF
RA3 = RA3 + DRAF*DSAF
231 DFCC= RA3/SQRT(RA1*RA2)
WRITE(6,56) DFCC
56 FORMAT(1H,10X,'CORRELATION COEFFICIENT (DAILY)',3X,F10.4)
232 CONTINUE
IF(CONOPT(5) .NE. 1) GO TO 233
  
```

```

C OUTPUT MAXIMUM RUNOFF, PRECIPITATION AT END OF YEARS
C
C
WRITE(6,57)
57 FCRMAT(1H,10X,'TWENTY HIGHEST CLOCKHOUR RAINFALL EVENTS IN THE
WATER YEAR')
WRITE(6,58) (T20PRH(KT20), KT20=1,20)
58 FCRMAT(1H,5X,20F6.3)
WRITE(6,59)
59 FCRMAT(1H,10X,'TWENTY HIGHEST CLOCKHOUR OVERLAND FLOW RUNOFF EV
ENTS IN THE WATER YEAR')
WRITE(6,58) (T20OFH(KT20), KT20=1,20)
233 CONTINUE
IF(CONOPT(6) .EQ. 0) GO TO 234
WRITE(6,60)
60 FCRMAT(1H1,30X,'DAILY SOIL MOISTURE OUTPUT ')
CALL DAYOUT(EDLZS,MEDWY,DPY)
234 CONTINUE
IF(CONOPT(10) .EQ. 1) GO TO 100
NOYR=NOYR-1
IF(NOYR.NE.0) GO TO 117
END
C *****
SUBROUTINE DAYNXT(DAY,DPY)
  
```

DYNX0002
 DYNX0003
 DYNX0004
 DYNX0005
 DYNX0006
 DYNX0007
 DYNX0008
 DYNX0009

 DYOT0001

DYOT0002

DYOT0003
 DYOT0004
 DYOT0005
 DYOT0006
 DYOT0007
 DYOT0008
 DYOT0009
 DYOT0010
 DYOT0011
 DYOT0012
 DYOT0013
 DYOT0014
 DYOT0015
 DYOT0016
 DYOT0017
 DYOT0018
 DYOT0019
 DYOT0020
 DYOT0021
 DYOT0022
 DYOT0023

C C DETERMINES NUMBER OF NEXT DAY OF THE YEAR
 C C

```

INTEGER DAY,DPY
DAY = DAY + 1
IF(DAY.EQ.366) DAY = 1
IF(DAY.EQ.6C.AND.DPY.EQ.366) DAY = 366
IF(DAY.EQ.367) DAY = 60
RETURN
END
*****
SUBROUTINE DAYOUT(VDCY,MEDWY,DPY)

```

C C PRINTS TABLE OF DAILY VALUES
 C C

```

DIMENSION MEDWY(12),VDCY(366),VDM(12)
INTEGER DATE,DAY,DPY
100 WRITE(6,1)
1 FORMAT(7X,'DAY',7X,'OCT',5X,'NOV',5X,'DEC',5X,'JAN',5X,'FEB',5X,
1 'MAR',5X,'APR',5X,'MAY',5X,'JUNE',5X,'JUL',5X,'AUG',5X,'SEPT',
MEDWY(3) = 0
DO 104 DATE = 1,28,1
IF(MOD(DATE,5).NE.1) GO TO 102
DO 101 KMD = 1,12
DAY = MEDWY(KMD) + DATE
101 VDM(KMD) = VDCY(DAY)
WRITE(6,2) DATE,VDM(12),(VDM(KWD), KWD=1,11)
2 FORMAT(1H,3X,I6,3X,12F8.1)
GO TO 104
102 DO 103 KMO = 1,12
DAY = MEDWY(KMO) + DATE
103 VDM(KMO) = VDCY(DAY)
WRITE(6,3) DATE,VDM(12),(VDM(KWD), KWD = 1,11)
3 FORMAT(1X,3X,I6,3X,12F8.1)
104 CONTINUE
IF(DPY.NE.366) GO TO 106

```

DYOT0024
 DYOT0025
 DYOT0026
 DYOT0027
 DYOT0028
 DYOT0029
 DYOT0030
 DYOT0031
 DYOT0032
 DYOT0033
 DYOT0034
 DYOT0035
 DYOT0036
 DYOT0037
 DYOT0038
 DYOT0039
 DYOT0040
 DYOT0041
 DYOT0042
 DYOT0043
 DYOT0044

 PREP0001
 PREP0002
 PREP0003
 PREP0004
 PREP0005
 PREP0006
 PREP0007
 PREP0008
 PREP0009
 PREP0010
 PREP0011
 PREP0012

```

DATE = 29
VDCY(60) = VDCY(366)
DO 105 KMD = 1,12
DAY = MEDWY(KMD) + DATE
105 VDM(D(KMD)) = VDCY(DAY)
WRITE(6,3) DATE,VDM(D(12)),(VDM(D(KMD)), KMD=1,11)
GO TO 107
106 CONTINUE
WRITE(6,4) VDCY(302),VDCY(333),VDCY(363),VDCY(29),VDCY(88),
1VDCY(119),VDCY(149),VDCY(180),VDCY(210),VDCY(241),VDCY(272)
4 FORMAT(1X,7X,29:3X,4F8.1,8X,7F8.1)
107 CONTINUE
108 WRITE(6,5) VDCY(303),VDCY(334),VDCY(364),VDCY(30),VDCY(89),
1VDCY(120),VDCY(150),VDCY(181),VDCY(211),VDCY(242),VDCY(273)
5 FORMAT(1X,7X,30:3X,4F8.1,8X,7F8.1)
WRITE(6,6) VDCY(304),VDCY(365),VDCY(31),VDCY(90),VDCY(151),
1VDCY(212),VDCY(243)
6 FORMAT(1X,7X,31:3X,4F8.1,8X,2F8.1,8X,F8.1,8X,F8.1,8X,2F8.1)
MEDWY(3) = 365
RETURN
END
*****
SUBROUTINE PREPRD(RGPM,DRHP,DAY,HOUR,DPY,PRD,PEP,PRH)
C *****
C DIVIDES HOURLY PRECIPITATION TOTALS AMNG PERIODS FOR SMALL BASINS
C
C DIMENSION DRHP(366,24), PE4P(4)
C INTEGER DAY,DPY,HOUR,PRD
C PEP = 0.0
C IF(PRH .EQ. 0.0) RETURN
C IF(PRD .EQ. 1) GO TO 100
C PEP = PE4P(PRD)
C RETURN
100 LHOURLY = HOUR - 1
LDAY = DAY
IF(LHOURLY .GE. 1) GO TO 101

```

```

LHOUR = 24
LDAY = DAY - 1
IF(LDAY .EQ. 0) LDAY = 365
IF(LDAY .EQ. 365) LDAY = 59
IF(LDAY .EQ. 59 .AND. DPY .EQ. 366) LDAY = 366
101 PRLH = RGPM*DRHP(LDAY,LHOUR)
    NHOUR = HOUR + 1
    NDAY = DAY
    IF(NHOUR .LE. 24) GO TO 102
    NHOUR = 1
    CALL DAYNXT(NDAY,DPY)
102 PRNH = RGPM*DRHP(NDAY,NHOUR)
    IF(PRH .GT. PRLH .AND. PRH .GT. PRNH) GO TO 103
    GO TO 104
103 PE4P(1) = 0.10
    PE4P(2) = 0.28
    PE4P(3) = 0.46
    PE4P(4) = 0.16
    GO TO 108
104 IF(PRH .LT. PRLH .AND. PRH .LT. PRNH) GO TO 105
    GO TO 106
105 PE4P(1) = 0.28
    PE4P(2) = 0.10
    PE4P(3) = 0.16
    PE4P(4) = 0.46
    GO TO 108
106 IF(PRNH .GE. PRLH) GO TO 107
    PE4P(1) = 0.46
    PE4P(2) = 0.16
    PE4P(3) = 0.28
    PE4P(4) = 0.10
    GO TO 108
107 PE4P(1) = 0.10
    PE4P(2) = 0.28
    PE4P(3) = 0.16
    PE4P(4) = 0.46
108 DO 109 KPRD = 1,4

```

```

PREP0013
PREP0014
PREP0015
PREP0016
PREP0017
PREP0018
PREP0019
PREP0020
PREP0021
PREP0022
PREP0023
PREP0024
PREP0025
PREP0026
PREP0027
PREP0028
PREP0029
PREP0030
PREP0031
PREP0032
PREP0033
PREP0034
PREP0035
PREP0036
PREP0037
PREP0038
PREP0039
PREP0040
PREP0041
PREP0042
PREP0043
PREP0044
PREP0045
PREP0046
PREP0047
PREP0048
PREP0049

```

PREP0050
PREP0051
PREP0052
PREP0053

RTVY0001
RTVY0002

109 PE4P(KPRD) = PE4P(KPRD)*PRH
PEP = PE4P(1)
RETURN
END

SUBROUTINE RTVARY(CTRI,SATRI,BTRI,CHCAP,NBTRI,MXTRI,NCTRI,EXQPV,
1 LSHFT,TEFCFS)

C
C
C

RTVY0003
RTVY0004
RTVY0005
RTVY0006
RTVY0007
RTVY0008
RTVY0009
RTVY0010
RTVY0011
RTVY0012
RTVY0013
RTVY0014
RTVY0015
RTVY0016
RTVY0017
RTVY0018
RTVY0019
RTVY0020
RTVY0021
RTVY0022
RTVY0023
RTVY0024
RTVY0025
RTVY0026
RTVY0027
RTVY0028
RTVY0029

DIMENSION ANSBIT(99),BTRI(99),CTRI(99),SATRI(99)
LOGICAL LSHFT
DO 100 KIA = 1,MXTRI
SATRI(KIA) = C.0
100 ANSBIT(KIA) = 0.0
LSHFT = .FALSE.
FMXTRI = MXTRI
FNBTRI = NBTRI
FNPTRI = NCTRI
TFX = TEFCFS
TFMRT = 0.1*CHCAP
IF(TFX.LT.TFMRT) TFX = TFMRT
IF(FNPTRI.EQ.FMXTRI.AND.TFX.EQ.TFMRT) RETURN
FNTRI = FNBTRI*(CHCAP/TFX)**EXQPV + 0.5
IF(FNTRI.LT.1.0) FNTRI = 1.01
NCTRI = FNTRI
FNSTRI = NCTRI
IF(FNSTRI.NE.FNPTRI) LSHFT = .TRUE.
IF(.NOT.LSHFT) RETURN
IF(FNPTRI.GT.98.5) GO TO 101
FCNTRI = ABS(FNSTRI - FNPTRI)
IF(FCNTRI.LE.1.1) GO TO 101
IF(FNSTRI.GT.FNPTRI) FNSTRI = FNPTRI + 1.0
IF(FNSTRI.LT.FNPTRI) FNSTRI = FNPTRI - 1.0
NCTRI = FNSTRI
101 KBI = 0
KB2 = 1

C
C
C

```

KB3 = 0
102 KBI = KBI + 1
    IF(KBI .GT. NBTRI) GO TO 105
KB4 = 0
WSBIT = BTRI(KBI)/FNSTRI
103 KB4 = KB4 + 1
    IF(KB4 .GT. NCTRI) GO TO 102
AWSBIT(KB2) = AWSBIT(KB2) + WSBIT
KB3 = KB3 + 1
    IF(KB3 .LT. NBTRI) GO TO 104
KB3 = 0
KB2 = KB2 + 1
104 GO TO 103
105 IF(FNPTRI .GT. 98.5) GO TO 108
    DO 107 KB6 = 1, NCTRI
    DO 106 KB7 = 1, KB6
106 SATRI(KB6) = SATRI(KB6) + AWSBIT(KB7) - CTRI(KB7)
107 CONTINUE
108 DO 109 KB5 = 1, MXTRI
109 CTRI(KB5) = AWSBIT(KB5)
    RETURN
    END
C *****
SUBROUTINE SNCMEL(BDDFSM, SPTWCC, SPM, ELDIF, DAY, SPBFLW, XDNFS, FFOR, SNOW0001
1  FFSI, MRNSM, DSMGH, SDEPTH, STMD, PXCASA, HOUR, SAX, SCFRF, OFRFIS, SOFRFI, SNOW0002
2  AMFSIL, PRH, SPTW, TANSM, SPLW, SFMD, OFRF, WT4AM, WT4PM, ASM, ASMRG, SNOW0003
3  SASFX, SARAX, DMXT, DMNT, RICY, FIRR) SNOW0004

```

```

C SNOWMELT CCPUTATION
C
C
C

```

```

DIMENSION DMNT(366), DMXT(366), FIRR(15), RICY(37)
INTEGER DAY, HOUR
REAL MHSM, MRNSM
IF((DAY .NE. 274) .OR. (HOUR .NE. 1)) GO TO 100
SPLW = 0.0
XELR = 0.0

```

```

RTVY0030
RTVY0031
RTVY0032
RTVY0033
RTVY0034
RTVY0035
RTVY0036
RTVY0037
RTVY0038
RTVY0039
RTVY0040
RTVY0041
RTVY0042
RTVY0043
RTVY0044
RTVY0045
RTVY0046
RTVY0047
RTVY0048
RTVY0049
RTVY0050
RTVY0051
*****
SNOW0005
SNOW0006
SNOW0007
SNOW0008
SNOW0009
SNOW0010
SNOW0011

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SNOW0012
 SNOW0013
 SNOW0014
 SNOW0015
 SNOW0016
 SNOW0017

SNOW0018
 SNOW0019

SNOW0020
 SNOW0021
 SNOW0022
 SNOW0023
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 SNOW0038
 SNOW0039
 SNOW0040
 SNOW0041
 SNOW0042
 SNOW0043
 SNOW0044

SNOW0045

SDSC = 0.0278
 FDSC = 0.0
 FTA = 0.0
 RICD = 0.0
 KRIA = 0

100 CONTINUE

C CALCULATION OF HCURLY AIR TEMPERATURE
 C DMXT CURRENT DAY, DMNT NEXT DAY
 C

IF(HOUR .NE. 4) GO TO 101
 FDSC = 0.0
 FTA = FDSC
 WT4PM = DMXT(DAY) - 4.0*ELDIF + (XELR/4.0)*0.7*ELDIF
 101 IF(HOUR .EQ. 10) SDSC = -0.0278
 IF(HOUR .EQ. 22) SDSC = 0.0278
 IF(HOUR .NE. 16) GO TO 102
 NDAY = DAY + 1
 IF(NDAY .EQ. 366) NDAY = 1
 IF(NDAY .EQ. 60 .AND. DMXT(366) .NE. 0.0) NDAY = 366
 IF(NDAY .EQ. 367) NDAY = 60
 WT4AM = DMNT(NDAY) - (XELR/4.0)*3.3*ELDIF
 102 IF(PRH .LE. 0.0 .OR. XELR .GE. 4.0) GO TO 103
 WT4AM = WT4AM - 0.825*ELDIF
 WT4PM = WT4PM + 0.175*ELDIF
 XELR = XELR + 1.0
 103 IF(PRH .NE. 0.0 .OR. XELR .LE. 0.0) GO TO 104
 WT4AM = WT4AM + 0.825*ELDIF
 WT4PM = WT4PM - 0.175*ELDIF
 XELR = XELR - 1.0
 104 TEH = WT4AM + FTA*(WT4PM - WT4AM)
 FDSC = FDSC + SDSC
 FTA = FTA + FDSC
 IF(PRH+SPTW .EQ. 0.0) GO TO 128
 IF(HOUR .NE. 24) GO TO 105

C CALCULATION OF TIME AGING OF THE SNOWPACK

SNOW0046
SNOW0047
SNOW0048

SAX = SAX + 1.0
IF(SAX .GT. 15.0) SAX = 15.0
105 IF(TEH .GT. 32.0) GO TO 110

C PRECIPITATION IN FORM OF SNOW - CALCULATE INTERCEPTION DENSITY OF NEWSNOW0049
C SNOW COMPACTION, AND SETTLING SNOW PACK AND THE EFFECT ON ALBEDO SNOW0050
C

IF(PRH .LE. 0.0) GO TO 110
PRH = SPM*PRH
HSF = PRH
ASM = ASM + HSF
PRH = (1.0 - (FFSI*FFOR))*PRH
HSFRG = PRH
ASMRG = ASMRG + HSFRG
FSIL = FFSI*FFOR*HSF
AMFSIL = AMFSIL + FSIL
IF(TEH .LE. 0.0) GO TO 106
DNFS = XDNFS + ((0.01*TEH)**2)
GO TO 107

106 DNFS = XDNFS
107 IF(SPTW .GT. 0.0 .AND. SDEPTH .GT. SPTW) SDEPTH = SDEPTH - ((PRH*
1 SDEPTH/SPTW)**(0.10*SDEPTH))*0.25))
SPTW = SPTW + PRH
SDEPTH = SDEPTH + (PRH/DNFS)
SASFX = SASFX + PRH
IF(SASFX .GE. PXCSEA) GO TO 108
GO TO 109

108 SAX = SAX - 1.0
IF(SAX .LT. 0.0) SAX = 0.0
SASFX = SASFX - PXCSEA
109 PRH = 0.0
110 CONTINUE
IF(SPTW .LE. 0.0) GO TO 127

C SEASONAL MELT FACTOR ADJUSTMENT
C
C

SNOW0077

SNOW0078
 SNOW0079
 SNOW0080
 SNOW0081
 SNOW0082
 SNOW0083
 SNOW0084
 SNOW0085
 SNOW0086
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 SNOW0088
 SNOW0089
 SNOW0090
 SNOW0091
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 SNOW0095
 SNOW0096
 SNOW0097
 SNOW0098
 SNOW0099
 SNOW0100
 SNOW0101
 SNOW0102
 SNOW0103
 SNOW0104
 SNOW0105
 SNOW0106
 SNOW0107
 SNOW0108
 SNOW0109
 SNOW0110

FDAY = DAY
 KAAO = KRIA
 KRIA = 1.0 + (FDAY/10.0)
 IF(KAAO .NE. KRIA) RICD = RICY(KRIA)
 IF(TEH .LE. 32.0) GO TO 111
 GO TO 114

C CALCULATION OF NEGATIVE MELT

111 IF(TANSM .LE. 11.5*MRNSM) GO TO 112
 IF(TANSM .LT. 1.0) TANSM = TANSM + ((5.0*MRNSM)**(1.3 + 2.0*
 1 TANSM))
 GO TO 113
 112 TANSM = TANSM + MRNSM
 113 IF(TANSM .GT. 0.08*SPTW) TANSM = 0.08*SPTW
 GO TO 127

C EFFECT OF RAIN ON ALBEDO

114 SARAX = SARAX + PRH
 IF(SARAX .LT. PXCSA/2.0) GO TO 115
 SAX = SAX + 1.0
 IF(SAX .GT. 15.0) SAX = 15.0
 SASFX = 0.0
 SARAX = SARAX - (PXCSA/2.0)
 115 IF(TEH .GT. 32.0) HSM = (TEH - 32.0)*BDDFSM
 IF(TEH .LT. 32.0) HSM = 0.0
 HSM = HSM*RICD

CAA = 1.0 + SAX
 IF(SAX .LT. 15.0) HSM = HSM*(1.0 - ((1.0 - FFOR)*FIRR(KAA)))
 IF(SAX .EQ. 15.0) HSM = HSM*(1.0 - ((1.0 - FFOR)*FIRR(15)))
 IF(PRH .GT. 0.0) HSM = HSM + ((TEH - 32.0)*(PRH/144.0))
 IF(STMD .GT. 0.3 .AND. SPTW .LT. SPTWCC) GO TO 116
 GO TO 117

116 MHSM = HSM
 HSM = (SPTW/SPTWCC)*HSM
 IF(HSM .LT. 0.1*MHSM) HSM = 0.1*MHSM

SNOW0111
 SNOW0112
 SNOW0113
 SNOW0114
 SNOW0115
 SNOW0116
 SNOW0117
 SNOW0118
 SNOW0119
 SNOW0120
 SNOW0121
 SNOW0122
 SNOW0123
 SNOW0124
 SNOW0125
 SNOW0126
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SNOW0136
 SNOW0137
 SNOW0138
 SNOW0139

SNOW0140
 SNOW0141
 SNOW0142
 SNOW0143

117 IF(HSM .LT. SPTW) GO TO 118

HSM = SPTW
 SDEPTH = 0.0
 SPTW = 0.0
 SPLW = 0.0
 RICD = 0.0
 TANSM = 0.0
 SAX = 15.0
 OFRF = SOFRF
 OFRFIS = SOFRFI
 GO TO 122

118 SPTW = SPTW - HSM
 IF(SFMD .LE. 0.0) GO TO 122
 IF(SAX .GE. 15.0) GO TO 121
 IF(SAX .GE. 6.0) GO TO 119
 SDEPTH = SDEPTH - (HSM/(0.5*SFMD))
 GO TO 122

119 IF(SAX .LE. 10.0) GO TO 120
 SDEPTH = SDEPTH - (HSM/(0.9*SFMD))
 GO TO 122

120 SDEPTH = SDEPTH - (HSM/(0.7*SFMD))
 GO TO 122

121 SDEPTH = SDEPTH - (HSM/SFMD)
 122 CONTINUE
 IF(SPTW .LT. 0.00001) SPTW = 0.0

C
 C CALCULATION OF LIQUID-WATER-HOLDING CAPACITY

C
 SPLWC = SPBFLW*SPTW
 IF(SFMD .GT. 0.6) SPLWC = SPBFLW*(3.0 - 3.33*SFMD)*SPTW
 IF(SPLWC .LT. 0.0) SPLWC = 0.0

C
 C ACCOUNTING OF MELT WATER AND RAIN
 C
 IF((SPLW + HSM + PRH) .GT. (SPLWC + TANSM)) GO TO 123
 GO TO 124
 123 PRH = HSM + PRH + SPLW - SPLWC - TANSM

SNOW0144
 SNOW0145
 SNOW0146
 SNOW0147
 SNOW0148
 SNOW0149
 SNOW0150
 SNOW0151
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SNOW0159

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 SNOW0166

SNOW0167

SNOW0168
 SNOW0169
 SNOW0170
 SNOW0171
 SNOW0172
 SNOW0173
 SNOW0174
 SNOW0175

```

SPLW = SPLWC
SPTW = SPTW + TANSM
TANSM = 0.0
GO TO 127
124 IF((HSM + PRH) .LE. TANSM) GO TO 126
125 SPTW = SPTW + TANSM
SPLW = SPLW + HSM + PRH - TANSM
PRH = 0.0
TANSM = 0.0
GO TO 127
126 TANSM = TANSM - HSM - PRH
SPTW = SPTW + HSM + PRH
PRH = 0.0
127 CONTINUE
HSM = 0.0

```

C CALCULATION OF DENSITY AND ADJUSTMENT OF OVERLAND FLOW TIME

```

C
C IF(SDEPTH .LE. 0.0 .OR. SPTW .GE. SDEPTH) GO TO 128
STMD = (SPTW + SPLW)/SDEPTH
SFMD = SPTW/SDEPTH
OFRF = 0.33*SOFRF
IF(SPTW .LE. SPTWCC) OFRF = (1.0 - (SPTW/SPTWCC))*SOFRF
128 IF(SDEPTH .LE. 0.0) OFRF = SOFRF
OFRFIS = SOFRF*OFRF/SOFRF

```

C CALCULATION OF GROUND MELT

```

C
C IF( HOUR .NE. 12 .OR. SPTW .LE. 0.0) RETURN
IF(SPTW .LE. DSMGH) GO TO 129
PRH = PRH + DSMGH
SPTW = SPTW - DSMGH
IF(STMD .LT. 0.50 .AND. SDEPTH .GT. 2.0*DSMGH) SDEPTH = SDEPTH -
1 2.0*DSMGH
RETURN
129 PRH = SPTW + PRH + SPLW

```

SNOW0176
SNOW0177
SNOW0178
SNOW0179
SNOW0180
SNOW0181
SNOW0182
SNOW0183
SNOW0184
SNOW0185

TANSM = 0.0
RICD = 0.0
SPLW = 0.0
SDEPTH = 0.0
SPTW = 0.0
SAX = 15.0
OFRF = SOFRF
OFRFIS = SOFRFI
RETURN
END

APPENDIX C

LISTING OF DATA CARDS FOR
1967-68 WATERYEAR

114
57

171 *pp*

01 *NCYR
 0 * OPTION 1, 1 IF 15-MINUTE STORM DETAILS ARE REQUESTED
 0 * OPTION 2, 1 IF RAIN IS NOT TO BE DIVIDED EQUALLY AMONG 15-MINUTE PERIODS
 1 * OPTION 3, 1 IF EVAPORATION IS READ BY 10-DAY PERIODS
 1 * OPTION 4, 1 IF DAILY FLOW ERROR TABLE IS REQUESTED
 1 * OPTION 5, 1 IF 20 TOP RAINFALLS AND OVERLAND FLOWS ARE REQUESTED
 1 * OPTION 6, 1 IF DAILY VALUES OF SOIL MOISTURE STORAGE ARE REQUESTED
 1 * OPTION 7, 1 IF SNOW IS TO BE INCLUDED IN ANALYSIS
 0 * OPTION 8, 1 IF THE STORAGE SITE MOVED DURING THE YEAR
 1 * OPTION 9, 1 IF DAILY RECORDED STREAM FLOWS ARE TO BE READ
 0 * OPTION 10, 1 IF NEXT YEAR OF DATA REQUIRES READING NEW WATERSHED PARAMETERS
 0 * OPTION 11, 1 IF DIVERSIONS ARE TO BE READ
 1 * OPTION 12, 1 IF STREAM ROUTING IS TO BE DONE HOURLY
 0 * OPTION 13, 1 IF LENGTH OF TIME-AREA-HISTOGRAM IS TO BE VARIED WITH FLOW
 1 * OPTION 14, 1 IF RECORDED STREAMFLOWS ARE TO BE PRINTED

NRTRI

25

0.0068	0.0163	0.0301	0.0331	0.0350	0.0512	0.0560	0.0551	0.0577	0.1033
0.0441	0.0309	0.0301	0.0349	0.0306	0.0350	0.0411	0.0358	0.0411	0.0577
0.0577	0.0551	0.0363	0.0161	0.0095					
0.50	0.50	0.45	0.40	0.35	0.30	0.25	0.20	0.15	0.10
0.55	0.56	0.57	0.61	0.67	0.75	0.80	0.83	0.87	0.92
0.96	0.99	1.00	1.00	0.98	0.95	0.91	0.87	0.84	0.81
0.79	0.77	0.75	0.73	0.72	0.71	0.70	0.69	0.68	0.67
0.65	0.64	0.62	0.60	0.57	0.56	0.55			
0.0000	0.0000	0.0000	0.049	0.046	0.045	0.045	0.050	0.046	* FALL
0.044	0.046	0.050	0.047	0.047	0.046	0.046	0.047	0.048	* WINTER
0.051	0.051	0.043	0.049	0.051	0.050	0.050	0.050	0.050	* SPRING
0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	* SUMMER
0.002	0.005	2.5	1.2	0.5	0.05	0.05	0.65	0.03	
0.0126	0.002	0.2							
1000.0		* RMPF							
1.0	317.0	0.0	0.0	0.0	0.0	0.0	0.0	0.30	6.0
0.15	1.0	0.60	7.4	0.27	0.0	0.0	0.0	0.30	5.5
0.29	1500.0	0.050	0.015	0.40					/FSS
0.95	0.97	2000.0	0.25	1.0	0.85				
0.02	0.0	4.0	0.02	0.0					

DEVELOPMENT OF SYNTHESIZED STREAM FLOWS FOR A REPRESENTATIVE YEAR

67 68

* WATER YEAR

PALOUSE RIVER NEAR POTLATCH, IDAHO

0.	12700.	11000.	08800.	05960.	06000.	04660.	03980.	03450.	0312		
0.	02830.	02780.	02880.	02970.	03160.	03260.	03500.	02880.	04550.	0720	
0.	09600.	12400.	19500.	19400.	20000.	20700.	24200.	19500.	26600.	2950	
0.	31800.	24200.	30400.	32000.	32100.	19800.	14300.	1310			
0.	85	0.90	0.60	0.40	0.25	0.40	0.60	0.70	0.75	0.80	0.85

* EPC 4

3.5
3.8
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6.6
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11.
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6.0
12.
4.7
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27.
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15.
2.2
4.7
5.4
8.5
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4.9
8.0
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8.8
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64.
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148.
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35. 23.
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30. 12.
28. 6.
28. 3.
26. 5.
17. 10.
26. 15.
31. 22.
26. 16.
18. 3.
25. 5.
36. 24.
41. 35.
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40. 34.
43. 33.
44. 32.
42. 34.
37. 30.
31. 27.
33. 29.
35. 17.
24. 5.
29. 7.
31. 16.
29. 10.
29. -5.
31. 15.
36. 14.
40. 21.
40. 25.
36. 23.
36. 12.
44. 33.
45. 33.
45. 35.
40. 30.

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KT20 = 20
194 IF(KT20 .LT. 1) GO TO 196
    IF(PRH .GT. T2OPRH(KT20)) GO TO 195
    T2OPRH(KT20 + 1) = PRH
    GO TO 197
195 T2OPRH(KT20+1) = T2OPRH(KT20)
    KT20 = KT20 - 1
    GO TO 194
196 T2OPRH(1) = PRH

C
C   ADDING GROUNDWATER FLOW
C
197 CBF = GWS*BFRL*(1.0 + BFNRL*BFNX)
    GWS = GWS - CBF
    AMBF = AMBF + CBF
    THGR = ARHF + CBF
    IF(HSE .GT. THGR) HSE = THGR
    AMSE = AMSE + HSE
    THSF(HOUR) = (THGR - HSE)*WCFS
    TDSF = TDSF + THSF(HOUR)

C
C   DRAINING OF UPPER ZONE STORAGE
C
UZINFX = (UZS/UZC) - (LZS/LZC)
IF(UZINFX .LE. 0.0) GO TO 198
LZSR = LZS/LZC
UZINLZ = 0.003*BMIR*UZC*UZINFX**3.0
IF(UZINLZ .GT. UZS) UZINLZ = UZS
UZS = UZS - UZINLZ
LZRX = 1.5*ABS(LZSR - 1.0) + 1.0
FMR = (1.0/(1.0 + LZRX))**LZRX
IF(LZS .LT. LZC) FMR = 1.0 - FMR*LZSR
PGW = (1.0-FMR)*UZINLZ*(1.0 - SUBWF)*FFPER
PLZS = FMR*UZINLZ
LZS = LZS + PLZS
GWS = GWS + PGW
BFNX = BFNX + PGW

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MAIN0527
MAIN0528
MAIN0529
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52. 36.
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51. 42.
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64. 31.
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73016710132	0.03	0.01	0.007				
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73016710212	0.02	0.02					
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73016710232	0.01	0.01					
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73016710272	0.03	0.03	0.03	0.03	0.03	0.03	0.03 0.03 0
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73016711 72							

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0.03 0.03			
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0.0180.018			
73016801162			
0.05			
73016801201			
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73016801301			
	0.07		
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0.12 0.03	0.07		
73016802032			
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73016802041			
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73016802172			
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73016802132			
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73016802191			
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0.01					
73016804052					
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73016804061					
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73016804062					
0.01	0.0060.01				
730168C4071					
	0.01				0.0040.004
73016804121					
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73016804122					
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73016804191					
					0.06
73016804201					
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0.0020.0020.0020.0020.0020.002					
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73016805142					
0.0070.007					0.01
73016805151					
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0.0010.0010.0010.0010.0010.001									
73016805201									
73016805202			0.04	0.01				0.13	0.14
0.18 0.01 0.005									
73016805211									
0.03									
73016805212									
73016805251									
73016805252									
0.06 0.04 0.03 0			0.02	0.02	0.04	0.04	0.03	0.01	0.02
73016805291									
73016806021									
0.0150.015									
73016806022									
0.02 0.02 0.03									
73016806051									
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73016806052									
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73016806071									
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73016806082									
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73016806112									
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73016806121									
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73016806122									

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73016807122		0.20	0.04	0.02
0.06				
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73016808101				
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0.0020.0020.0020.002				
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73016808132				
0.02		0.02		
73016808141				
	0.01	0.02	0.01	0.02
73016808142				
0.01 0.02 0.01 0.02 0.01 0.01				
73016808151				
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0.0010.0010.0010.0010.001				
73016808162				
0.0010.0010.0010.0010.001				
73016808201				
	0.03	0.03		

73016808202					
73016808211			0.01	0.03	0.03
0.02	0.01				
73016808241		0.02	0.02	0.02	0.02
73016808242			0.03	0.03	0.03
0.03	0.03	0.01			
73016808262					
73016808271		0.0050	0.005		
73016808272			0.0050	0.0050	0.0050
73016808281					
0.110					
73016809121					
0.0050	0.0050	0.0050	0.0050	0.0050	0.0050
73016809132					
73016809141		0.04	0.01		0.02
0.20	0.30	0.16	0.04		
73016809142					
73016809151				0.20	0.04
0.01					
73016809152			0.01		
0.04					
73016809171				0.0040	0.0040
73016809172					
73016809181				0.0020	0.0040
0.10	0.25	0.12	0.20	0.14	0.12
73016809182					
73016809191					0.06
					0.02

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0.0010.0010.0010.0010.0010.0010.0010.0010.0010.0010.0010

73016809201

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73016809202

0.05 0.02 0.03

0.02 0.0 0.01 0.01

73016809211

0.0060.04

0.01 0.01 0.0080.008 0.008

73016809212

0.02

0.04 0.04

0.0080.008

73016809221

0.14 0.07

73019809301

APPENDIX D
OUTPUT FOR THE PALOUSE RIVER
FOR THE 1967-68 WATERYEAR

// ASSGN SYS002,X'00C'
// ASSGN SYS003,X'00E'
// EXEC

CONTROL OPTION CODE TABLE

* 0 * OPTION 1 *
* 0 * OPTION 2 *
* 1 * OPTION 3 *
* 1 * OPTION 4 *
* 1 * OPTION 5 *
* 1 * OPTION 6 *
* 1 * OPTION 7 *
* 0 * OPTION 8 *
* 1 * OPTION 9 *
* 0 * OPTION 10 *
* 0 * OPTION 11 *
* 1 * OPTION 12 *
* 0 * OPTION 13 *
* 1 * OPTION 14 *

34. 29.
42. 30.
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48. 35.
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47. 34.
42. 25.
29. 16.
17. 7.
27. 7.
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32. 23.
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DEVELOPMENT OF SYNTHESIZED STREAM FLOWS FOR A REPRESENTATIVE YEAR

PALOUSE RIVER NEAR POTLATCH, IDAHO
 WATER YEAR 1967-68

MONTH	DATE	DEPTH	STMD	SAX	TANSM	SPLW								
NOVEMBER	29	SDEPTH=	0.39	STMD=	0.19	SAX=	15.00	TANSM=	0.01	SPLW=	0.00			
DECEMBER	4	SDEPTH=	0.16	STMD=	0.15	SAX=	15.00	TANSM=	0.00	SPLW=	0.00			
	5	SDEPTH=	0.73	STMD=	0.21	SAX=	15.00	TANSM=	0.01	SPLW=	0.01			
	6	SDEPTH=	0.47	STMD=	0.19	SAX=	15.00	TANSM=	0.01	SPLW=	0.01			
	7	SDEPTH=	0.30	STMD=	0.19	SAX=	15.00	TANSM=	0.01	SPLW=	0.01			
	8	SDEPTH=	0.61	STMD=	0.17	SAX=	15.00	TANSM=	0.01	SPLW=	0.01			
	9	SDEPTH=	0.97	STMD=	0.19	SAX=	15.00	TANSM=	0.00	SPLW=	0.01			
	10	SDEPTH=	0.03	STMD=	0.16	SAX=	15.00	TANSM=	0.00	SPLW=	0.00			
	16	SDEPTH=	0.52	STMD=	0.05	SAX=	15.00	TANSM=	0.00	SPLW=	0.00			
	17	SDEPTH=	0.48	STMD=	0.01	SAX=	15.00	TANSM=	0.00	SPLW=	0.00			
	19	SDEPTH=	1.77	STMD=	0.10	SAX=	15.00	TANSM=	0.01	SPLW=	0.00			
	20	SDEPTH=	1.43	STMD=	0.09	SAX=	15.00	TANSM=	0.01	SPLW=	0.00			
	21	SDEPTH=	1.14	STMD=	0.12	SAX=	15.00	TANSM=	0.01	SPLW=	0.00			
	22	SDEPTH=	2.77	STMD=	0.22	SAX=	15.00	TANSM=	0.00	SPLW=	0.03			
	23	SDEPTH=	2.70	STMD=	0.22	SAX=	15.00	TANSM=	0.00	SPLW=	0.03			
	24	SDEPTH=	2.56	STMD=	0.22	SAX=	15.00	TANSM=	0.00	SPLW=	0.03			
	25	AM	426.4	457.9	491.2	540.8	573.6	619.2	671.6	742.8	824.7	909.4	940.6	980.3

PM 1021.3 1072.6 1133.1 1201.4 1275.9 1356.1 1440.6 1525.6 1605.0 1676.8 1742.1 1802.6 1043.2
MAXIMUM= 1323.6 C.F.S. TIME 12.00 P.M.
25 SDEPTH= 2.43 STMD= 0.21 SAX= 15.00 TANSW= 0.0 SPLW= 0.02

26 AM 1859.9 1914.4 1966.4 2015.7 2063.0 2111.1 2153.3 2188.8 2214.3 2228.3 2230.8 2237.4

PM 2226.9 2204.2 2175.3 2144.5 2109.6 2077.5 2038.5 1998.2 1956.9 1914.9 1872.6 1830.2 2072.2
MAXIMUM= 2231.8 C.F.S. TIME 10.45 A.M.
26 SDEPTH= 1.74 STMD= 0.20 SAX= 15.00 TANSW= 0.0 SPLW= 0.02

27 AM 1789.1 1747.9 1707.6 1668.2 1629.8 1592.4 1556.1 1520.8 1486.6 1453.5 1421.4 1393.2

P4 1366.5 1342.3 1310.1 1296.7 1274.9 1253.5 1232.4 1211.6 1191.0 1170.2 1149.6 1129.2 1412.6
 MAXIMUM= 1805.8 C.F.S. TIME 0.15 A.M.
 27 SDEPTH= 1.18 STWD= 0.23 SAX= 15.00 TANSW= 0.0 SPLW= 0.01

28 AM 1109.0 1085.3 1070.0 1051.4 1033.5 1016.3 1000.1 984.7 970.3 957.1 944.8 943.5

PM 933.3 923.2 913.7 904.6 895.6 886.4 877.0 867.4 857.3 846.6 835.6 824.9 947.3
 MAXIMUM= 1110.0 C.F.S. TIME 0.15 A.M.
 28 SDEPTH= 0.55 STWD= 0.22 SAX= 15.00 TANSW= 0.01 SPLW= 0.01
 29 SDEPTH= 0.19 STWD= 0.20 SAX= 15.00 TANSW= 0.00 SPLW= 0.00
 30 SDEPTH= 0.15 STWD= 0.12 SAX= 15.00 TANSW= 0.00 SPLW= 0.00
 31 SDEPTH= 0.47 STWD= 0.15 SAX= 15.00 TANSW= 0.01 SPLW= 0.00

JANUARY
 1 SDEPTH= 2.71 STWD= 0.11 SAX= 14.00 TANSW= 0.02 SPLW= 0.00
 2 SDEPTH= 2.28 STWD= 0.11 SAX= 15.00 TANSW= 0.02 SPLW= 0.00
 3 SDEPTH= 1.83 STWD= 0.10 SAX= 15.00 TANSW= 0.01 SPLW= 0.00
 4 SDEPTH= 1.35 STWD= 0.09 SAX= 15.00 TANSW= 0.01 SPLW= 0.00
 5 SDEPTH= 1.54 STWD= 0.08 SAX= 15.00 TANSW= 0.01 SPLW= 0.00
 6 SDEPTH= 0.95 STWD= 0.06 SAX= 15.00 TANSW= 0.00 SPLW= 0.00
 8 SDEPTH= 0.74 STWD= 0.14 SAX= 15.00 TANSW= 0.01 SPLW= 0.00
 9 SDEPTH= 1.59 STWD= 0.18 SAX= 15.00 TANSW= 0.02 SPLW= 0.01
 10 SDEPTH= 2.56 STWD= 0.21 SAX= 15.00 TANSW= 0.04 SPLW= 0.02
 11 SDEPTH= 2.38 STWD= 0.21 SAX= 15.00 TANSW= 0.04 SPLW= 0.02
 12 SDEPTH= 2.00 STWD= 0.21 SAX= 15.00 TANSW= 0.01 SPLW= 0.02
 13 SDEPTH= 1.25 STWD= 0.21 SAX= 15.00 TANSW= 0.00 SPLW= 0.01
 14 SDEPTH= 0.34 STWD= 0.20 SAX= 15.00 TANSW= 0.00 SPLW= 0.00
 30 SDEPTH= 0.50 STWD= 0.10 SAX= 15.00 TANSW= 0.00 SPLW= 0.00

FEBRUARY
 13 AM 293.1 320.5 350.7 371.5 388.8 407.8 427.9 449.1 471.0 495.1 519.8 549.5

PM 590.1 629.5 679.3 729.5 793.9 863.9 923.9 993.5 1068.5 1146.8 1215.3 1261.8 664.2
 MAXIMUM= 1257.3 C.F.S. TIME 12.00 P.M.
 19 AM 1324.7 1373.6 1427.8 1473.9 1524.5 1590.7 1674.5 1732.4 1787.9 1850.6 1923.3 2002.7

PM 2100.1 2196.4 2292.8 2395.6 2503.5 2599.8 2722.7 2844.9 2973.4 3073.8 3221.4 3373.2 2166.0
 MAXIMUM= 3366.1 C.F.S. TIME 12.00 P.M.
 20 AM 3503.6 3651.1 3741.4 3825.8 3905.1 3980.0 4051.6 4122.5 4194.6 4269.3 4345.7 4422.2

PM 4496.3 4564.8 4625.1 4675.1 4713.3 4739.0 4752.2 4753.9 4745.1 4726.6 4758.0 4778.4 4347.5
MAXIMUM= 4765.9 C.F.S. TIME 7.00 P.M.

21 AM 4776.6 4796.6 4765.9 4743.7 4708.2 4712.2 4725.1 4733.5 4758.5 4786.8 4812.1 4820.7

PM 4803.2 4789.1 4778.9 4774.0 4775.0 4780.6 4791.5 4807.1 4825.4 4843.3 4857.5 4866.4 4784.2
MAXIMUM= 4882.6 C.F.S. TIME 12.00 P.M.

22 AM 4868.7 4864.6 4854.9 4840.6 4822.5 4800.8 4774.9 4744.1 4707.3 4663.8 4613.4 4556.6

PM	4527.2	4468.3	4398.0	4324.8	4249.7	4172.9	4095.3	4017.3	3938.8	3865.5	3782.8	3699.1	4443.8
	MAXIMUM=	4982.4	C.F.S.	TIME	1.00	A.M.							
23	AM	3614.6	3530.0	3448.7	3365.9	3313.6	3292.5	3274.5	3260.5	3249.6	3190.5	3139.7	3097.7
	PM	3065.0	3041.8	3027.9	3023.9	3028.8	3039.5	3051.7	3061.9	3068.5	3072.1	3073.5	3073.7
		MAXIMUM=	3651.6	C.F.S.	TIME	0.15	A.M.						3183.6
24	AM	3073.3	3073.5	3075.5	3080.3	3087.1	3093.3	3095.6	3091.1	3078.5	3057.8	3029.7	2995.7
	PM	2956.8	2914.2	2868.7	2821.1	2772.1	2722.0	2671.4	2620.8	2570.4	2520.5	2471.3	2422.9
		MAXIMUM=	3107.7	C.F.S.	TIME	7.00	A.M.						2981.8
25	AM	2375.5	2329.1	2283.8	2239.7	2196.8	2155.0	2114.4	2075.0	2036.8	1999.6	1963.6	1928.7

PM 1894.8 1861.9 1830.0 1799.1 1769.1 1739.9 1711.5 1683.9 1657.2 1631.2 1606.0 1581.5 1936.0
MAXIMUM= 2398.2 C.F.S. TIME 0.15 A.M.

26 AM 1557.7 1534.6 1512.1 1490.2 1468.9 1448.2 1428.1 1408.4 1389.4 1370.8 1352.6 1335.0
PM 1317.8 1301.0 1284.7 1268.7 1253.2 1237.9 1223.0 1208.5 1194.2 1180.4 1166.8 1153.5 1336.9
MAXIMUM= 1571.1 C.F.S. TIME 0.15 A.M.

27 AM 1140.6 1127.9 1115.5 1103.4 1091.5 1079.9 1068.5 1057.4 1046.4 1035.7 1025.3 1015.0
PM 1004.9 975.0 985.3 975.8 966.4 957.2 948.2 939.3 930.5 921.9 913.5 905.2 1014.6
MAXIMUM= 1149.4 C.F.S. TIME 0.15 A.M.

MARCH 13 SDEPTH= 0.10 STMD= 0.14 SAX= 15.00 TANSM= 0.00 SPLW= 0.0

25 AM 74.7 74.2 73.7 73.2 72.7 72.2 71.8 71.3 70.8 132.9 165.8 232.5

PM 292.9 313.5 353.7 408.0 475.4 552.5 639.7 750.2 855.8 949.9 1034.6 1112.2 371.4
MAXIMUM= 1141.4 C.F.S. TIME 12.00 P.M.

26 AM 1181.9 1246.4 1309.0 1367.7 1425.6 1489.3 1557.3 1626.6 1688.6 1735.8 1767.7 1787.6

PM 1800.2 1801.7 1803.5 1778.3 1747.9 1713.6 1676.5 1637.5 1597.2 1556.4 1515.4 1474.5 1595.3
MAXIMUM= 1795.8 C.F.S. TIME 1.15 P.M.

27 AM 1434.0 1394.0 1354.6 1316.0 1278.2 1241.4 1205.5 1170.6 1136.8 1104.1 1072.4 1041.9

DATE: 1-1-68
 TIME: 0.15 A.M.
 092.6 829.6 805.4 783.0 761.4 740.4 1049.2

MAY 5 SDEPTH= 0.08 STRD= 0.15 SAX= 15.00 TANSM= 0.00 SPLW= 0.0

JUNE
 JULY
 AUGUST
 SEPTEMBER

DEVELOPMENT OF SYNTHESIZED STREAM FLOWS FOR A REPRESENTATIVE YEAR
 PALOUSE RIVER NEAR POTLATCH, IDAHO
 WATER YEAR 1967-68
 KENTUCKY WATERSHED MODEL

DAY	RECORDED FLOWS											
	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN*	JUL	AUG	SEPT
1	3.5	14.0	16.0	63.0	53.0	438.0	210.0	78.0	56.0	10.0	4.2	4.0
2	3.8	12.0	16.0	52.0	65.0	407.0	210.0	73.0	30.0	10.0	3.9	7.4
3	4.7	11.0	14.0	34.0	183.0	368.0	212.0	72.0	17.0	10.0	3.6	9.1
4	6.6	15.0	14.0	47.0	268.0	345.0	183.0	73.0	28.0	10.0	3.6	3.9
5	15.0	3.1	24.0	46.0	348.0	342.0	188.0	60.0	32.0	10.0	3.8	3.5
6	21.0	1.9	17.0	30.0	272.0	318.0	232.0	63.0	34.0	9.0	3.8	3.3
7	20.0	5.1	30.0	32.0	208.0	282.0	230.0	63.0	33.0	8.0	2.5	4.8
8	11.0	8.8	28.0	32.0	181.0	250.0	230.0	58.0	65.0	7.0	2.5	2.6
9	3.5	9.4	17.0	33.0	137.0	222.0	210.0	44.0	12.0	6.0	3.1	2.6
10	6.0	13.0	18.0	37.0	106.0	185.0	195.0	54.0	32.0	4.0	2.5	3.4
11	12.0	54.0	17.0	46.0	115.0	165.0	185.0	50.0	30.0	5.2	2.0	3.0
12	4.7	59.0	17.0	43.0	92.0	154.0	173.0	53.0	32.0	8.0	2.2	3.0
13	10.0	28.0	15.0	49.0	69.0	158.0	173.0	45.0	33.0	6.3	2.5	3.3
14	27.0	24.0	16.0	42.0	67.0	171.0	158.0	48.0	31.0	14.0	2.6	6.8
15	24.0	32.0	18.0	124.0	77.0	167.0	152.0	47.0	28.0	11.0	2.5	6.6
16	24.0	24.0	13.0	122.0	69.0	159.0	154.0	55.0	27.0	8.8	2.5	11.0
17	15.0	22.0	4.5	102.0	69.0	173.0	141.0	46.0	21.0	8.2	3.0	19.0
18	2.2	29.0	4.7	92.0	302.0	160.0	137.0	34.0	19.0	5.8	3.1	30.0
19	4.7	19.0	7.7	77.0	344.0	146.0	130.0	38.0	17.0	5.4	5.1	94.0
20	5.4	8.2	10.0	32.0	544.0	132.0	137.0	39.0	16.0	8.0	5.6	70.0
21	8.5	12.0	10.0	82.0	413.0	126.0	122.0	54.0	15.0	4.0	3.5	49.0
22	4.7	14.0	14.0	176.0	347.0	119.0	115.0	66.0	35.0	10.0	8.0	56.0
23	4.9	15.0	122.0	154.0	242.0	119.0	112.0	57.0	30.0	5.8	5.4	52.0
24	9.0	11.0	184.0	137.0	220.0	112.0	105.0	38.0	25.0	6.6	10.0	43.0
25	12.0	17.0	765.0	119.0	134.0	116.0	103.0	57.0	20.0	7.4	6.3	30.0
26	8.0	11.0	366.0	97.0	914.0	193.0	102.0	48.0	16.0	3.8	3.4	26.0
27	8.8	8.8	228.0	65.0	707.0	195.0	108.0	61.0	14.0	3.6	7.3	22.0
28	20.0	6.0	148.0	69.0	569.0	325.0	96.0	54.0	13.0	3.1	8.8	21.0
29	64.0	12.0	110.0	63.0	487.0	305.0	78.0	52.0	12.0	4.0	9.2	13.0
30	32.0	14.0	38.0	67.0		262.0	78.0	44.0	11.0	5.1	19.0	13.0
31	23.0		57.0	59.0		230.0		38.0		4.0	16.0	11.0

DAY	DAILY SCIL MOISTURE OUTPUT											
	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN*	JUL	AUG	SEPT
1	4.0	3.9	4.5	7.0	7.6	9.1	9.3	9.1	9.1	9.1	7.6	2.4
2	4.0	3.9	4.5	7.0	7.6	9.1	9.3	9.1	9.1	9.1	7.6	2.4
3	4.0	3.9	4.6	7.1	7.7	9.1	9.3	9.0	9.0	9.0	7.6	2.3
4	4.0	3.9	4.7	7.1	7.8	9.1	9.3	8.9	8.9	8.9	7.5	2.3
5	3.9	3.9	4.8	7.1	7.8	9.1	9.4	8.8	8.8	8.8	7.4	2.2
6	3.9	3.9	4.9	7.1	7.8	9.1	9.4	8.7	8.7	8.7	7.4	2.2
7	3.8	3.9	4.9	7.1	7.8	9.1	9.4	8.6	8.6	8.6	7.3	2.1
8	3.7	3.9	4.9	7.1	7.8	9.1	9.4	8.5	8.5	8.5	7.3	2.1
9	3.7	4.0	4.9	7.1	7.8	9.1	9.4	8.5	8.5	8.5	7.3	2.1
10	3.6	4.2	5.0	7.1	7.8	9.1	9.4	8.4	8.4	8.4	7.3	2.0
11	3.6	4.2	5.0	7.1	7.8	9.1	9.4	8.4	8.4	8.4	7.3	2.0
12	3.6	4.3	5.1	7.1	7.8	9.1	9.4	8.3	8.3	8.3	7.3	2.0
13	3.6	4.4	5.1	7.2	7.8	9.1	9.4	8.2	8.2	8.2	7.3	2.0
14	3.6	4.5	5.1	7.3	7.8	9.2	9.4	8.1	8.1	8.1	7.3	2.0
15	3.5	4.5	5.1	7.5	7.8	9.2	9.4	8.1	8.1	8.1	7.2	2.0
16	3.6	4.5	5.1	7.5	7.8	9.2	9.4	8.0	8.0	8.0	7.1	2.0
17	3.5	4.5	5.1	7.5	7.9	9.2	9.4	7.9	7.9	7.9	7.0	2.0
18	3.5	4.5	5.1	7.5	8.2	9.2	9.4	7.8	7.8	7.8	6.9	2.0
19	3.5	4.5	5.1	7.5	8.6	9.2	9.4	7.7	7.7	7.7	6.8	2.0
20	3.4	4.5	5.1	7.5	8.7	9.2	9.4	7.7	7.7	7.7	6.7	2.0
21	3.4	4.5	5.1	7.5	9.0	9.2	9.4	7.8	7.8	7.8	6.6	2.0
22	3.5	4.5	5.3	7.6	9.0	9.2	9.4	7.8	7.8	7.8	6.5	2.0
23	3.5	4.5	5.6	7.6	9.1	9.2	9.4	7.8	7.8	7.8	6.5	2.0
24	3.5	4.5	5.8	7.6	9.1	9.2	9.4	7.8	7.8	7.8	6.5	2.0
25	3.5	4.5	6.7	7.6	9.1	9.3	9.4	7.8	7.8	7.8	6.4	2.0
26	3.5	4.5	6.8	7.6	9.1	9.3	9.4	7.8	7.8	7.8	6.3	2.0
27	3.5	4.5	6.9	7.6	9.1	9.3	9.3	7.8	7.8	7.8	6.2	2.0
28	3.9	4.5	7.0	7.6	9.1	9.3	9.3	7.8	7.8	7.8	6.2	2.0
29	3.9	4.5	7.0	7.6	9.1	9.3	9.2	7.8	7.8	7.8	6.2	2.0
30	3.9	4.5	7.0	7.6	9.1	9.3	9.2	7.8	7.8	7.8	6.2	2.0
31	3.9	4.5	7.0	7.6	9.1	9.3	9.2	7.7	7.7	7.7	6.1	2.0

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