Research Topics: 1. Cascaded queucing systems in manufacturing 2. Coercivity in polycrstalline thin films 3. AWDI and Wiggle in metal film heads 3. AWDI and Wiggle in metal film heads 3. Coerclary corollary: Domain wall motion in metal film heads
1. Cascaded quencing systems in manufacturing
2. Coercivity in polycrstalline thin films
3. AWDI and wiggle in metal film heads
-> Constany corollary: Domain wall motion in metal film head
4. Partial response signaling in magnetic recording
5. Adaptive signal processing in magnetic recording
6. Quantum Theory of ferromagnetic carbon
7. Effects of imperfectly modeled resonance in a
variable structure control system
8. Can raw data error rate be improved using
nomilinear filtering? (Idea is a compressor -expander
nonlinear filtering? (Idea is a compressor-expander) to boost peaks and suppress inflexions
9. Modeling vibration amplification in mechanism
shock mounted in a cabinet tolinducture
shock mounted in a cabinet mutual inductance mutual inductance 10. Calculation of coefficient of acoupling in
printed circuits
11. Effect of above-Nyquist resonances in
sampled control system
12. Quantum mechanics of 2 interacting particles in a box
13, Grain boundary effect on free electrons in a simple metal
14. Modeling of free electron gas in a ferromagnetic metal
(continue : can free electrons in a metal be
(modeled as a quantum change distribution?)
7591169

15. Effects of start strategy in mufe's system (Konbon, etc) 16. Effect of rework flow on an usveribly line 17. Effects of station downtime on an assoubly tine that response signation in magneticanil 18. Batch minguent strategies in an assembly process 19. Failure analysis/ disposition queues effects on production Thruput lindude effects of multiple faults and mis-diagnosis) 20. Effects of interpolation and 1st order holds in Olzital control systems 21. Battleneck strategies in assembly processes 22. Thermal muguent of scretace mount components 23. Optimal ITAE compensation of resonant systems 24. Molelly noise and transducer noise in adaptive control systems 25. Error correcting codes in servo field applications 26. Weighing a moving semi using road-embedded yord sensore of pitardis & to produce material II 13 Gerain boundary effect of free electrons in a single week 14. Modeling of free electron pas in a ferromagnetic meetal (was fire electrons in a metal be (very delad as a Euradium change distribution?)

$$\lambda_{L} = 0, 1 \quad f_{2}Q_{1} = \begin{bmatrix} 1 & 1 \end{bmatrix} T$$

$$\lambda_{2} = 1.0 \quad f_{2}Q_{2} = \begin{bmatrix} 1-1 \end{bmatrix} T$$

$$\int_{11}^{1} + \int_{12}^{1} = 0.1 \quad f_{21}^{1} + f_{22}^{1} = 0.1$$

$$\int_{11}^{1} + \int_{12}^{1} = 0.1 \quad f_{21}^{1} + f_{22}^{1} = 0.1$$

$$\int_{11}^{1} - \int_{12}^{1} = +1.0 \quad f_{21}^{1} + f_{22}^{2} = -1.0$$

$$\Rightarrow f_{11} = 0.55 \quad f_{21}^{2} = -0.45$$

$$\int_{12}^{1} = -0.45 \quad f_{22}^{2} = +0.55$$

$$\Theta = \begin{bmatrix} 1 & 0 \end{bmatrix}^{\frac{1}{2}} \Rightarrow \begin{bmatrix} .55 & -45 \\ -.45 & .55 \end{bmatrix} \begin{bmatrix} 0 \\ -.65 \end{bmatrix} = \begin{bmatrix} 0.25 \\ -.275 \end{bmatrix} = .001375$$

$$\Theta = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} .55 & -45 \\ -.45 & .55 \end{bmatrix} \begin{bmatrix} 0 \\ -.45 \end{bmatrix} = \begin{bmatrix} 0.55 \\ -.45 \end{bmatrix} = 0.55$$

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1.591169

1, = 0, t 1, 0 = 1, 1 [1-1]= 103/ 1001 = 56 Put 1/2 = 0.1 - 1/2 = 0.4 ≈ Pu = 0.55 Pu = -0.45 34.00 = 19 [2(4+2)2)20 + 2620) = = 430200 [2(4+20)]700 = $\left[\frac{3(w,w)}{9+} + \frac{1}{9} + \frac{1}$] = | 1 | 22,0 2 (+ (w.-w) + + (w.-w) +) = = Lut (166 34 9) 2 = 5wt 9 (24 3w) 5w D [0,10] = [05.] = [1,1 20] = [1,1 20] = = [1 1.] [1-1] 2 = [1-1] [55 - 55.] [1-1] 7 [1 1.] [1-1] 2 = [1-1] [55 - 55.] [1 1] 7 1x2.0-1x22, 4x22. ~ YSZ.+ YXZA.- YXZA. - [YZZ. = [YZZ.+ XZA.-][XX]

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5/n(wt) = cor (wt - 17/2)
  cuz(\omega t + \omega) = \frac{1}{2} \left[ e^{j(\omega t + \omega)} - \frac{1}{2}(\omega t + \omega) \right]
= \frac{1}{2} \left[ e^{j\omega t} - \frac{1}{2}\omega t - \frac{1}{2}\omega t \right]
      = \frac{1}{2} \left( \text{corb} + j \text{sinb} \right) \right + \left( \text{corb} - j \text{sinb} \right) \right) \right = \frac{1}{2} \text{corb} \left[ \right( \text{e}^{j\text{orb}} \right] + \frac{1}{2} \text{sinb} \left[ \right( \text{e}^{j\text{orb}} \right] - \right( \text{e}^{j\text{orb}} \right) \right]
     = cor 0 cor(wt) - sin 0 sin wt
 : s(t) = a(t) cor (wt+0)
                  = (a(t) coro) corot - (a(t) sino) sinut
                   = X(t) wrwt - y(t) sin wt
    phaser:
                                         u(t)
                                                                 u(t) = x(t) + j y(t)
  The definitions
               finitions
((f-f_c) \stackrel{d}{=} \begin{cases} H(f), f>0 \\ 0, f<0 \end{cases} \stackrel{H(f)}{=} \begin{cases} 1 \\ 0 \end{cases}
              C^*(-f-f_c) = {\begin{cases} H^*(-f), f > 0 \\ f < 0 \end{cases}}
 in motivated by the fact that

a(t) e just puduces only positive frequencies
  for xample
 a(t) = a c \omega x \omega t \Rightarrow a(t) e^{j \omega_z t} = \frac{q}{2} \left( e^{j (\omega_z + \omega)t} + e^{j (\omega_z - \omega)t} \right)
 and the output of a BPF has the form
                   r(t) = Re [v(t) e imit]
when represented in complex envelope form. Then
                      v(t) = u(t) * c(t) w c(t) = 7 { ((+)}
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5/7 (wt) = was (wt - 17/2) 2KB | 5, [1787] 2, [27/27] 22 (27/27) 27 から一つから」の対と多十「から」のがかっ ((°7-7) 2 XKB 50 [(°7-7)] CUS (Z# f. (4-4)) (57-7) Jus (57-7) 12 (57-7) 07 c3 / (4) gaz 1 101 chook this in my note: moth problem: S(w). o + dutinal (m) H = (m) H + (m) H (m) 8 + = (m) -2 X(w) = (w) X = (w) X またいかります。 a(19) = 1 a core up to 10 (14) e 1(m) H at the act for the free the (1/4) par H(w) = K[(4-4)/8) + post ((4+4)/B)] = 1 wto

$$g(t) = 2kB \int \frac{\sin(\pi B \tau)}{\pi B \tau} \cos(2\pi f_{\epsilon} \tau) d\tau$$

$$= KB \int \frac{\sin(\pi G f_{\epsilon} + B)\tau}{\pi B \tau} \int \sin(\pi (B - 2f_{\epsilon})\tau) d\tau$$

$$= K(2f_{\epsilon} + B) \int \frac{\sin(\pi (2f_{\epsilon} + B)\tau)}{\pi (2f_{\epsilon} + B)\tau} d\tau$$

$$= K(2f_{\epsilon} + B) \int \frac{\sin(\pi (2f_{\epsilon} + B)\tau)}{\pi (2f_{\epsilon} + B)\tau} d\tau$$

$$= K(2f_{\epsilon} + B) \int \frac{1}{2} \int \frac{\sin(\pi (2f_{\epsilon} + B)\tau)}{\pi (2f_{\epsilon} + B)\tau} d\tau$$

$$= K(2f_{\epsilon} + B) \int \frac{1}{2} \int \frac{1}{2}$$